

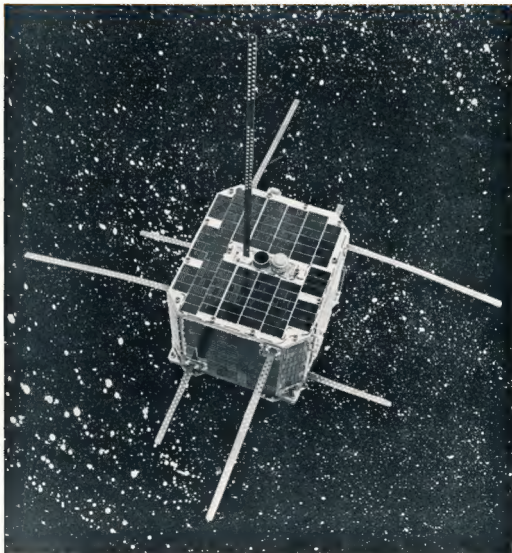
amateur radio

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JULY, 1970

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COVER STORY

An artist's impression of the type of satellite that OSCAR 6 will probably be. The surface of the package is covered with solar cells, which should give the satellite an active life of at least one year.

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For further information contact—

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Telephone 620131



W.I.A.'s Preliminary Comments on the 1971 Space Frequency Conference

Previous Federal Comments and the last Annual Report of the Federal Executive have referred to the 1971 World Administrative Radio Conference relating to space services.

The Federal Executive, on behalf of the Federal Council, has now submitted to the Australian Administration the preliminary comments of the W.I.A. in relation to the forthcoming Conference.

Having regard to what I consider to be the importance of this initial statement, this Federal Comment is devoted to the full text of it.

—Michael J. Owen, VK3KI,
Federal President, W.I.A.

1. WIRELESS INSTITUTE OF AUSTRALIA

The Wireless Institute of Australia (W.I.A.) is the single body representing Amateur Radio in Australia. Just over one half of all enthusiasts in Australia are members. The W.I.A. is a member of the International Amateur Radio Union (I.A.R.U.), a world-wide organisation made up of the National Amateur Radio Societies of 53 countries and administrations throughout the world. Through this organisation the W.I.A. is aware of the views being put forward by the forthcoming World Administrative Radio Conference in many countries. In addition, the W.I.A. has been responsible for the inauguration of an association of National Amateur Radio Societies within Region 3 under the auspices of I.A.R.U. At present the W.I.A. is providing a Secretariat for this organisation.

In addition, it is directly interested in the utilisation of radio for space purposes as it includes within it the W.I.A. Project Astronaut Group, the group responsible for designing and constructing the Amateur Satellite Australia OSCAR 5.

2. RADIO AMATEURS AND SPACE COMMUNICATION

The following extracts from Docket No. 18294 submitted to the Federal Communications Commission on 29th April, 1970, by the American Radio Relay League (A.R.R.L.) and the Radio Amateur Satellite Corporation (A.M.S.A.T.) are of interest in the present context:

"Radio Amateurs have played a most important role in the development of space exploration and communication. In recent years, two organisations (in the United States) of dedicated Radio Amateurs, working in their spare time and without compensation other than the personal pleasure that comes from making contributions to society, have made most significant contributions to the development of the space techniques and experience. The first was Project OSCAR Inc.—OSCAR means 'Orbital Satellite Carrying Amateur Radio'—organised in 1960 by the Radio Amateurs of the United States. The second, A.M.S.A.T., was organised early in 1969 by Amateurs engaged in space research and development at Washington, D.C. A.M.S.A.T.'s purpose is to foster world-wide Radio Amateur participation in space experiments and in so doing, bring and maintain the best communications for Amateurs and other services alike.

"Many of A.M.S.A.T.'s members have extensive experience in space telecommunications technology and its member organisations are Amateurs in over twenty countries. The international aspect of Amateur Radio space activities was expanded just three months ago when A.M.S.A.T. in co-operation with the National Aeronautics and Space Administration (N.A.S.A.), arranged for the testing and launch of an Amateur Satellite designed and constructed by a group of Radio Amateurs in Australia. Australia's OSCAR 5 was placed in orbit in January 1970. The satellite is the most advanced Amateur satellite, and has also submitted a proposal to N.A.S.A. to provide two communications experiments to be carried on the ATS-G Application Technology Satellite.

"Amateur satellite work has been typified by a variety of configurations, from the relatively unsophisticated ground stations, such as are operated by Amateurs around the world. This approach has made Amateur satellite work a truly international venture in

keeping with the United Nations General Assembly Resolution 1721 (XVI) Part D and 1802 (XVII) Part IV paragraph 3, which expresses the belief that 'communications satellites should be organised on a global basis with non-discriminatory access for all nations'."

In Australia the encouragement given to the Amateur Service by the World Administrative Radio Conference (W.A.R.C.) for the utilisation of space techniques is of special significance for the present W.I.A. Project Astronauts provides one of the very few opportunities for Australians to participate in the use of space for communications. It should be noted that Australia's OSCAR 5 was only the second Australian designed and built satellite to "fly", and the first to be constructed primarily of Australian components.

Accordingly, the W.I.A. most strongly urges that it is in the national interest to encourage the development of the Amateur Radio Service, particularly in space.

As is pointed out by A.R.R.L. and A.M.S.A.T., Amateur Radio is far more than hobbyists talking amongst themselves; it is a direct road to self-sustaining communications systems without which no nation can progress, a comment of particular significance in Australia.

3. THE AMATEUR SERVICE FREQUENCY REQUIREMENTS

The W.I.A. recognises the pressures on the frequency spectrum caused by the ever-growing requirements of all services. In the context of the Amateur Service, the density of use in terms of numbers of actual stations operating regularly and irregularly within a specific allocation is no measure of the importance of the allocation to the service—at least in the v.h.f. and higher bands, for, as these frequencies are used, a broad frequency spectrum are regularly used. (For example, Amateur I.v. is a feature of Amateur activity.) It is not necessary to list the many group activities and in the Institute's view should be encouraged.

The utilisation of bands higher than 144-148 MHz. for space communications will undoubtedly encourage greater utilisation of these bands by Amateurs generally.

This incentive to use higher frequencies will in turn be encouraged by the increasing availability of suitable low cost components for use by Amateurs at these higher frequencies. Whilst the W.I.A. does not see any increase in the existing allocations, it does not believe that there should be, on the other hand, any curtailment of these allocations.

4. SPACE USAGE BY THE AMATEUR SERVICE

Footnote 284A of the Radio Regulations 1969 states: "In the band 144-148 Mc/s, artificial satellites may be used by the Amateur Service."

In the W.I.A.'s view the concept of the Amateur Service is certainly broad enough to include such use. The definition of the service adopted by the Regulations certainly does not imply any restriction on the use of frequencies. However, the existence of the footnote has been thought to imply that such use is not permitted on other OSCAR 5 transmitted on a frequency of 29.450 MHz; OSCAR 4 transmitted on a frequency of 431.935 MHz. These transmissions were permitted by the Regulations which permits the use of any frequency if it does not result in interference. There is, therefore, pressure for the use of frequencies outside the band 144-148 MHz. for Amateur satellite use.

The following bands are exclusively allocated to the Amateur Service on the basis of 7.0-7.1 MHz., 14.0-14.35 MHz., 21.0-21.45 MHz., 28.0-28.7 MHz., 144.0-148.0 MHz.

The Radio Regulations of the I.T.U. provide for shared use by Amateurs of other bands throughout the spectrum from 1.8 MHz. to 22.0 GHz.

In relation to the exclusive bands, Amateurs have the potential of interfering only with other Amateurs. Most of the exclusive allocations are at lower frequencies. Even though propagation of radio waves at these frequencies are well known for terrestrial communication, only limited experiments have been conducted at these frequencies using transmitters in space. Satellites operating at these frequencies will provide a valuable tool for further research into ionospheric ducting, absorption, atmospheric propagation, and other effects, etc. The Amateur Service, with hun-

dreds of thousands of experienced Radio operators in every part of the world is particularly well equipped to gather this sort of information. The type of investigation are, of course, of universal significance.

By Joint Docket No. 18294, the A.R.R.L. and A.M.S.A.T. have commented to the Federal Communications Commission:

"With respect to the exclusive world-wide Amateur bands, A.R.R.L. and A.M.S.A.T. urge that we limit the frequency allocation to the forthcoming W.A.R.C. for space operations. Such a policy will provide each administration with the greatest possible flexibility to encourage or restrict Amateur use of development."

The W.I.A. adopts this suggestion and comments it to the Australian Administration.

5. THE PROBLEM OF SHARED BANDS

Certain terrestrial experiments (such as moon bounce on the 70 centimetre band and higher allocations utilising high power) and certain fixed installations such as beacons and repeaters and communications through satellites could conceivably present special problems in shared bands. Interference from normal Amateur operations above 100 MHz. is not a problem for terrestrial stations. The same techniques for point to point communication, present no special problem, as in fact interference from the Amateur Service is not presented difficulties in the past and can in any event be easily controlled.

Up-link communications from an Amateur station transmitting a satellite in the Amateur Service should, the W.I.A. contends, be permitted in any Amateur band regardless of whether it is shared, provided the terrestrial stations' transmissions are in accordance with the Regulations of the country in which it is located.

However, in relation to the utilisation of the existing shared bands for down-links and the other special requirements of the Amateur Service, the W.I.A. contends, if it is added, could conceivably present special problems. The W.I.A. contends that these problems would be removed, if within the shared bands, an exclusive allocation for the Amateur Service were made. Such a course would seem to offer the best solution to the Amateur Service's requirements. The Amateur Service, which is easily controlled, and its requirements for specialised experiments that appear to be currently present administrations with a problem of interference with other services having higher priority. In making this suggestion and in relation to the Institute's proposals for the use of shared bands, it should be pointed out that the possibility of interference from Amateur satellites is, in fact, remote.

OSCAR 4, launched on 21st December, 1965, into a highly elliptical, 28 degrees synchronous transfer orbit contained a 5-watt transmitter operating on 431.935 MHz. There are no known reports of interference to the radio-location service from this transmitter.

It should also be borne in mind that it is unlikely that the terrestrial antennas used in the radio-location and radio navigation services would be aimed at an Amateur satellite. These antennas are designed to receive signals from a rotating type, the main lobe of which would be, at worst, only briefly exposed to satellite energy; the narrow beamwidths of these antennas also tend to minimise the exposure time.

Having regard to the already envisaged utilisation of Amateur satellites in television experiments an exclusive allocation at 70 centimetres of 10 MHz. would appear to be essential. The W.I.A. is accordingly strongly recommending the allocation of this band to the Amateur Service's shared bands.

6. AN ADDITIONAL PROPOSAL

Even if the foregoing primary submission of the W.I.A. finds favour, it is considered that an additional utilisation of shared bands should be permitted for space communications, though it is recognised that the frequency allocation must be provided to provide compliance with the priorities applicable to each band should harmful interference be caused. The feasibility of reliable telecommunication a shift in carrier frequency, a reduction in power or a change in the type of antenna as well as the ceasing of emission altogether. The frequency allocation to the Australian OSCAR 3 experiments in January and February 1970. The transmitter in the metre band is expected to be put off to operate on a regular week-end schedule.

(Continued on Page 25)

An Integrated Circuit One Watt Audio Amplifier

J. REYNOLDS,* VK3ZMU

The amplifier described will deliver one watt r.m.s. audio power into a capacitively coupled 8 ohm speaker, using a 12v. supply. Maximum power to a 16 ohm speaker is approximately one half watt at 12v. supply, or one watt at 16v. The frequency response may be made very wide for hi-fi use or tailored for communication purposes. Gain of the amplifier is adjustable so that full output may be obtained for input voltages in the range 15 mV. to 200 mV. r.m.s.

The input circuit uses a common emitter CR coupled transistor amplifier with negative feedback. This is coupled to a Motorola integrated circuit type MC1454G which raises the power level to one watt. Because of the small value electrolytic capacitors required, capability of 12v. operation and gain adjustment facility, this circuit has proved to be more useful in many Amateur applications than circuits using the less expensive TAA300.

THE CIRCUIT

Fig. 1 shows the circuit of the complete amplifier. Audio input is coupled to the base of the transistor amplifier through C1, a 0.22 μ F. polyester capacitor. A.C. negative feedback results from R4 and the unbypassed portion of VR1 in the emitter circuit. By varying the unbypassed portion of VR1, gain can be controlled without disturbing the d.c. bias conditions. R4 is necessary to maintain a high input impedance.

For the ME1001 transistor, the input impedance is about 8K ohms with VR1 fully bypassed and about 85K ohms with no bypassing. A high input impedance is necessary because C1, in series with the input impedance of the stage, forms a high pass filter and thus determines low frequency response. Also, if the emitter was fully bypassed, a high impedance driving source would be required to reduce distortion due to non-linearity of the transfer conductance. This is an undesirable restriction.

The gain of the stage may be varied between 1 and 12 by adjustment of VR1. The amplified signal is capacitively coupled from the collector load resistor (2.7K ohms) to the input of the integrated circuit. C4 and R3 (in parallel with the input impedance of the IC) form a low pass filter and thus determine the high frequency response of the amplifier. The input impedance of the IC is approximately 10K ohms. With C4 equal to 0.02 μ F., a bandwidth of 4 KHz. is obtained. This may be increased to 13 KHz. by reducing C4 to 0.002 μ F.

The circuit of the IC is shown in Fig. 2. The gain of the IC is controlled and stabilised against temperature and component variations by a conventional method adopted with differential input operational amplifiers. With these amplifiers the differential (emitter coupled) transistors act in antiphase, that is, one inverts the input and the other is non inverting. The gain of the op.

amp. will stabilise when the inverting and non-inverting inputs are of equal magnitude.

If one input is fed with the signal and the other is connected to the output via a voltage divider of, say, 10:1, the input voltages will not be equal until the output voltage is 10 times the input voltage. Thus by fixing one resistor in the divider and varying the other the amplifier gain can be varied.

In the MC1454G these resistors are internal. The fixed resistor connected to the output is 10K ohms and goes to the non-inverting input. From the non-inverting input there is a selection of shunting resistors to a.c. ground. By varying the combination of resistors by-passed, the gain of the IC can be adjusted to the discrete values of 10, 18 or 36. In this design a gain of 18

was selected as the best compromise between gain and distortion.

The output stage is two Darlington pairs in conventional configuration. Output power is capacitively coupled to a speaker via C9, a 100 μ F. 16 v.w. electrolytic capacitor. The value of C9 also effects the low frequency response of the amplifier, however with the value of C1 specified, the effect of C1 predominates.

The transistors in this integrated circuit exhibit considerable gain up to v.h.f. To avoid v.h.f. instability, CR stabilising networks (0.04 μ F. in series with 10 ohms) are connected from pins 9 and 10 to ground. C10 shown in the circuit diagram acts as a reservoir capacitor to supply the peak current demands of the amplifier. This is only necessary when the amplifier is used

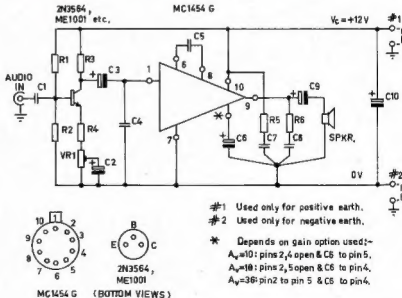


FIG. 1—IC, AUDIO AMPLIFIER CIRCUIT.

R1—100K ohms.
R2—47K ohms.
R3—2.7K ohms.
R4—120 ohms.
R5—10 ohms.
VR1—2K ohms.
C1—0.22 μ F.
C2—50 μ F., 10 v.w.

C3—5 μ F., 25 v.w.
C4—see text.
C5—39 μ F.
C6—50 μ F., 10 v.w.
C7, C8—0.04 μ F.
C9—100 μ F.
C10—100-1500 μ F. (if required).

* 4 Balmoral Avenue, Kew, Vic. 3101.

with a poorly regulated power supply or flat battery. Provision for this capacitor has not been made on the printed circuit board.

PERFORMANCE

Fig. 4 shows the measured frequency response of the amplifier. The effect of gain adjustment on the low frequency response can be seen. The high frequency response falls at 20 dB per decade. The slope of this roll-off can be increased to 40 dB per decade by connecting a suitable capacitor from pin 6 to ground. Suggested values are 0.01 μ F. for a bandwidth of 3.5 KHz. and 0.002 μ F. for a bandwidth of 13 KHz.

Fig. 3 shows total harmonic distortion plotted against power output.

Typical performance figures are:

Nominal supply voltage: 12V.

Bandwidth:

120 Hz.-13 KHz. (min. gain, C4 0.005 μ F.)

170 Hz.-13 KHz. (max. gain, C4 0.005 μ F.)

160 Hz.-4.5 KHz.

(max. gain, C4 0.02 μ F.)

Sensitivity: 14 mV. r.m.s. input required to produce 1W. r.m.s. output power into an 8-ohm speaker.

Distortion: less than 0.8% between 60 mW. and 0.8 W.; less than 2% between zero and 1 W.

Operating supply voltage: 6-13.5V. (more than 100 mW., 8 ohms); 7-18V. (more than 100 mW., 16 ohms).

Zero signal current drain: less than 20 mA.

Input impedance: 8K ohms (max. gain); 35K ohms (min. gain).

Maximum power output: 1.2 W. (with heat sink).

CONSTRUCTION

The circuit is constructed on a 4 cm. x 8 cm. fibre glass printed circuit board. VR1 is a miniature pre-set potentiometer. Provision has been made for either positive or negative earth, as selected by straps.

DIDDLY DAH DIT

Further experience with the IC Keyer described recently in "A.R." shows that insufficient filtering in an a.c. to d.c. supply has the effect of distorting the leading edge of the timing pulses. Hum, together with poor power supply regulation causes occasional errors at the start of a dash sequence, making the first dash sometimes appear as a dot. Providing the at-rest d.c. supply voltage is at least 3 volts, a drop of $\frac{1}{2}$ volt is not likely to cause any problem. A simple zener regulated supply capable of 80 mA. is therefore satisfactory. Providing a large value capacitor is used after a dropping resistor, there is no reason why a smallish resistor cannot be used in the supply line to "trim" the d.c. supply to the design centre value of 3 $\frac{1}{2}$ volts.

There have been some reports of r.f. on the keying line causing a continuous key-down condition. This can be minimised by using r.f. chokes in the keying lines; by normal shielding and bypass procedures; and by modification of the keyer to add a 1 μ F. tantalum 3 $\frac{1}{2}$ volt working capacitor between the base of the transistor switch and chassis. This will also serve (with the 1K feed resistor) to integrate the switching pulses to sawtooth shape, which seems to provide a slightly more acceptable keying characteristic. The capacitor should not be less than 0.5 μ F. if hum spikes on the keying pulses are to be eliminated.

Contrary to some opinions, the keyer does produce dashes which are self-completing, but not all dots are self-completing. The first and last dots in a dot sequence can be shortened by premature paddle movement—not so the dashes. Recognition of this feature helps to know how to free the paddle so as to send error-free (almost) auto Morse. By increasing the resistance of the speed control potentiometer the "speed" can be lowered and the self-completing dash feature demonstrated.

Having tried both breadboard and printed board construction, it is clear that the printed board method is by far the best. If anyone needs a board, similar to the one used by "QST," I can probably arrange supply of a commercially made board at cost on request. At last quote, \$1 plus postage.

—Col Harvey, VK1AU

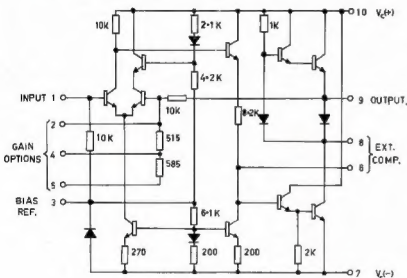


FIG. 2 - SCHEMATIC OF MC14546 AUDIO I.C.

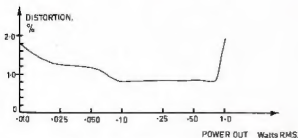


FIG. 3 - I.C. AUDIO AMPLIFIER: DISTORTION.

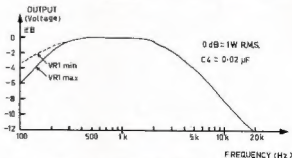


FIG. 4 - I.C. AUDIO AMPLIFIER: FREQUENCY RESPONSE.

Modifications to the FL200B Yaesu Musen Transmitter

R. D. CHAMPNESS,* VK3UG

Since obtaining this transmitter about 3½ years ago the author has learnt much about the art of SSB and in particular about this particular variety of transmitter. The modifications described are a mixture of necessities and personal choices.

THE lay-out of the audio input from the microphone socket to the grid of the microphone pre-amplifier is quite poor. The mic. socket is right alongside the mains on-off switch and the whole of the audio input lead of about 4 inches is unshielded. In my transmitter this resulted in hum modulation of my signal. To overcome this, the lead was shielded and a shield tube was made out of tinfoil to go completely over the mic. socket, which cured this fault.

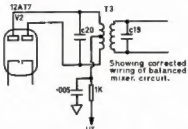
It is most disconcerting on vox operation to hear the relays clanking in and out, and as well, it meant that the vox had to be desensitised as the noise of the relays operating caused the transmitter to cut in and out of operation. To overcome this fault I rubber-mounted the two relays. The one in the p.a. cage I mounted on a grommet which fitted into an enlarged hole in the side of the cage. For the relay on the rear apron of the chassis, I cut small rubber washers which were fitted on both sides of the chassis wall. The original screw would not fit (too short) so a couple of nuts were soldered to the relay and some longer screws used to mount the relay. By doing this, the noise of relays was considerably reduced, so making vox operation easier.

I had much trouble on c.w. with the key contacts fouling up. This was so bad that I had to clean the contacts after every QSO, and boy that should not be necessary, and is a sign of rather poor design. The reason for this poor performance lies in the fact that when the key is depressed it shorts out some of the grid blocking bias system, which is a very effective method of keying, but the key in this case directly shorts out C43, C58, C67 and C98, which means the key discharges these capacitors in microseconds from a voltage of about -120 volts to zero. This adds up to 0.065 µF.

To reduce this sparking and fouling of the key contacts two 1K resistors are fitted in series with the capacitors in a particular way. One resistor is fitted in the vertical line at the extreme right of the circuit and the other is fitted in the bias line immediately above the caption "V8 12BY7A" on the circuit. By inserting these two resistors the operation of the keying circuit is unaffected but the peak keying current across the key contacts is reduced to 300 mA., and continuous key down current is 8 mA. The value of these resistors is not critical but I would not go below the value I used.

I fitted these resistors, one on the tag strip by the p.a. tube bases, there is a

spare lug. The white wire is the lead that is cut to fit the resistor. The other resistor is fitted near the 6CB6 V7. Once again there is a spare lug. There are three white wires with blue traces. The one coming from the centre part of the transmitter chassis is broken to fit the resistor.



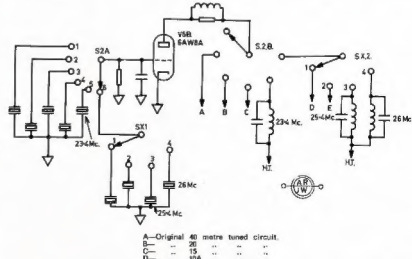
I had trouble with vox and keying circuit giving unreliable operation and traced this to R31, a 1 watt 50K resistor. This resistor had succumbed to its overload so two 82K ohm 1 watt resistors in parallel were fitted, making this section much more reliable. The 50K, or 47K as it was marked, was dissipating nearly two watts. Bad design I feel.

Should you ever burn out a 6BM8 voltage regulator consider fitting a 6CV8 as it has a much higher heater-cathode rating. The 6BM8 has only 100 volts

rating and in the voltage regulator it has 150 volts between these two elements. See my article on voltage regulators in "A.R." Dec. 1969.

Much to my surprise, one day I observed the 12BY7A driver glowing red hot. I immediately thought that something was wrong and started to delve into the works, but on going through the valve voltage chart I found all voltages to be normal. However, when I checked the ratings of the valve I found that in this circuit it is being overrun by about 60%. The screen voltage, for instance, is 280 volts, whereas data on the valve indicates a maximum of 190 volts. I did quite a bit of experimenting about this stage, but found that it worked best with the circuit as is. The valves must be rugged as I haven't blown one yet. I can't say I am happy with the valve being overrun like this, but it seems to keep going quite okay.

This transmitter has rather limited coverage of 10 metres, only going from 27.9 to 29.1 MHz. To overcome this I have thought of fitting an extra switch to bring in other crystals when the band switch gets to position 10B. The 10A position could be used for the 11 m.e. (26.96 to 27.23 MHz.) band. As per accompanying diagram, at least another two h.f. bands would be achieved with little problem. The switch could be fitted on the front panel in much the same way as done for the



S2 will now read: 80-40-20-15-11-10. SX1 will read 10A, 10B, 10C, 10D, so covering all 10 metres. In the plate circuit of V8 (6AW8A) the wiring would be altered as for S2B and S2C but the tuned circuits would tune for 11 metres 32.4 MHz., 10 metres C 34.4 MHz., and 10 metres D 35 MHz.

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FT200. I have not done this particular mod., but am thinking about doing it.

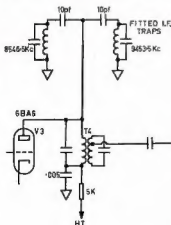
The tuning of the rig on 80 metres in particular, to me, was unsatisfactory; the loading capacitor was at maximum capacity and yet the loading capacitor seemed to need more capacity. I took off the bottom cover of the cage and found I could fit an extra loading capacitor to the 80 metre circuit. I fitted an extra 330 pF. to the contact shown on switch S2F nearest the bridged 10 metre tank coil contacts on the circuit, or if you observe looking down into the upturned chassis, the contact to solder to is the one second from the bottom on the side of the wafer nearest the centre of the transmitter chassis.

I also found it desirable to shift the 80 and 40 metre tank coil tapplings. I shifted the 80 metre tapping along 4 turns, giving more inductance, and the 40 metre one 2 turns to give more inductance. The loading of the transmitter is now more satisfactory and the r.f. output, particularly on 80 metres, is greatly improved.

Whenever I switched the unit on the transformer would make a bit of a protest as the electrolytic capacitors were charged up. To overcome this, I fitted a CZ11A thermistor in series with the transformer. The transformer protest ceased, the diodes had less peak current to handle, and the fuse was able to be reduced to 2 amps. very comfortably instead of the 3 amps. originally. It should be possible to run even as light as 1.5 amps.

There are a couple of circuit drawing errors I have found and these I have shown in corrected form in a couple of small diagrams. One concerns the balanced mixer V2 and the other the plate circuit of V6A. There are a few minor differences in various FL200 circuits, so some of the things I have drawn to your attention may not even be in your set, or some of the mods., for all I know, may be in the set. Thus it is best that you peruse your set before doing anything to it.

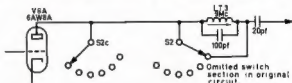
I have fitted three other traps to the transmitter in addition to the ones already fitted. In the plate circuit of the 6BA6 9 MHz. i.f. amplifier, I fitted



traps to reduce the crystal oscillator frequencies of 8546.5 KHz. and 9453.5 KHz. I'm not really sure how effective these have proved to be as I have not a general coverage receiver to check the suppression of these frequencies in the i.f. amplifier. These can show up as spots 453.5 KHz. away from the desired output frequency of the transmitter.

I was troubled with spurious spots on 7 MHz. and I know for a fact mine is not the only one like this. What I did was to fit a 6.8 MHz. trap in series with LT3 and by careful tuning using a receiver tuned to 6.8 MHz. I was able to reduce this particular spot. This one is caused by the second harmonic of the 3.4 MHz. crystal oscillator on 40 metres. Fred VK3YS suggested this particular trap.

The traps are tuned to the following frequencies: LT1 6.8 MHz., LT2 9 MHz., LT3 9 MHz. LT3 is not mentioned in the alignment data of the transmitter



at all. I found that the method outlined in the alignment data did not give very accurate alignment of the traps and I did them the following way. On 14 MHz. I tuned up the transmitter on 14.250. I then ran it on net with full carrier inserted and tuned my receiver to 14.150. You will then find a small carrier which can be nulled out by adjustment of LT2 and LT3. LT3 is under the chassis.

The 9 MHz. i.f. is heterodyned with a 10.4 MHz. crystal to give 19.4 MHz. which is then heterodyned with, say, the v.f.o. at 5.15 MHz. to give 19.4 - 5.15, giving 14.250. But the weak 9 MHz. signal in the plate circuit can also beat with 5.15 MHz. and give 9 + 5.15 = 14.15 MHz. So it can be seen why these traps are in there.

To adjust the 6.8 MHz. traps get hold of a receiver than can tune 6.8 MHz. and set the transmitter up on 40 and then tune in the net position of the transmitter LT1 for least 6.8 MHz. signal in the receiver. Also, if you fit the additional 6.8 MHz. trap I fitted, adjust this for minimum signal. The rest of the transmitter tuning is more or less as per book.

I would suggest that the balanced modulator be tuned up listening on a receiver to the transmitted frequency. There will be a small whistle if the balanced modulator is not quite balanced. Adjust the trimmer and pot alternatively for minimum whistle. It should be possible to virtually eliminate the carrier altogether and all you will be left with will be some mushy 50 and 100 cycle sounds and their harmonics.

The Yaesu Musen transmitters are renowned for their excellent carrier suppression. I doubt that even the so-

called Rolls Royce of s.s.b. gear, the Collins, can beat them on this score. I purposely have not given data on the coils used in the traps but suggest you follow the general style of the existing traps in the unit.

I felt that the transmitter was not complete without some additional metering, such as the screen voltage, screen current of the final, a.c. operation, and p.a. h.t. voltage. A tx monitor as I called it, was built which consisted of a 5-position switch, a few resistors and a 1 mA. meter. The actual construction and circuit details can be seen in "A.R.", Dec. 1969, in the article "Sideband The Expensive Way (How to avoid it)". The miniature 5-pin socket was mounted on the rear apron of the chassis alongside the bias pot where the extension a.c. socket was mounted.

In conclusion, I might comment that I have learnt a great deal about sideband from working on this and one or

two other sideband rigs and in general have found it most educational. The modifications I have done won't upset your re-sale value as there is very little sign of anything having been done to the set, certainly nothing externally although no sensible modification should cause any deterioration in the value of the rig, possibly the reverse. Do not throw the old cliché at me that "to do any alterations to a rig would spoil the re-sale of it". The re-sale of any rig is not high, so why not have it working as it should, and better, then you won't want to sell it.

Have fun with the rig, I have. It is not perfect, but then what rig is, and if it was, we wouldn't learn very much about it because nothing would go wrong, and Murphy's Law has not been disproved yet!!!

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THE "M.C.M." OR MOVING COIL METER

K. A. KIMBERLEY, VK2PY

To most radio enthusiasts the ubiquitous moving coil meter (M.C.M.) is a standard item around the workshop. Useful as it is, some of us tend to accept it at face value without ever wondering how or why it works. The purpose of this article is not to engage in a erudite discussion but rather to present the basic principles as simply as possible

THE operating principle of all meters is fundamentally similar in that the quantity to be measured is converted into a mechanical force capable of moving an indicating system.

There are many types of meters manufactured, each with its own special characteristics, thus making some types more suitable for some applications than others. Some that come to mind are:—

- (1) Moving coil (M.C.M.).
- (2) Moving iron.
- (3) Electrostatic.
- (4) Hot wire, etc.

However, for this article I will confine myself to the moving coil meter as it is the most commonly used type in the electronics game.

Some of us know it as the "D'Arsonval" and it consists essentially of a coil of wire suspended within the field of a permanent magnet. An indicator attached to the coil points to a numbered scale.

Direct current, on passing through the coil, produces a flux field which acts with that of the magnet to produce a physical movement. As will be explained later, this movement is proportional to the current flow, hence the scale may be directly calibrated in terms of current, etc.

So much for the intro, now to detail the various parts of the M.C.M.

MAGNET AND POLE PIECES

Pre-war meters, as well as today's cheaper types, used a conventional hardened steel horseshoe magnet. These were reasonably satisfactory due to the care taken in the aging process.

As one would expect, WW2 saw the invention and development of many exotic alloys. One such was "Alnico" which contains aluminium, nickel, cobalt, steel and copper. Alnico has some exceptional magnetic properties, among which are:

- (1) Magnetic susceptibility (μ_r).
- (2) High retentivity (B_r).
- (3) High coercive force (H_c).

The above refer to the amount of magnetism resulting from a given input and the ability to retain it over a long period under normal conditions.

Mechanically it is a hard brittle crystalline metal and is extremely difficult to machine, and for this reason Alnico is generally cast. Finishing is normally confined to grinding.

Iron pole pieces are attached to the magnet and are so shaped as to leave a circular air gap in which the coil is suspended. A soft iron core is fitted

into the centre of the gap, leaving a cylindrical space in which the coil moves on its axis.

The magnetic lines of force are now radial to the centre of the soft iron core. Ideally all of the lines of force should be of the same length and hence the field would be of uniform intensity. However, this is not always so and is caused by the cylindrical walls not being perfectly co-axial. Imperfections such as high and/or low spots will also distort the field.

The aberrations mentioned above are the major causes of scale non-linearity.

A slotted triangular shaped piece of ferrous metal is sometimes fitted across portion of the air gap to provide a means of adjusting the flux density. This is called a magnetic shunt and is used to adjust the final sensitivity of the meter movement. It may also be used as a means to compensate for magnet aging.

COIL

In a practical meter this consists of many turns of fine copper wire wound on a lightweight former. For a given magnet assembly the number of turns governs the sensitivity in terms of current and hence voltage.

That is, the 1 mA-100 ohm milliammeter, which is probably one of the most commonly used meters in Australia, would need, as per Ohm's Law, 0.1v. (100 mV.) for full scale deflection (f.s.d.).

Now if we double the number of turns, then 0.5 mA. will be required for f.s.d. Now the d.c. resistance will then be increased to more than double (that sounds Irish, but nevertheless is true). However, let us assume that the resistance has been in fact doubled, we will find that 0.1v. will still be required for f.s.d.

Keeping the original number of turns but increasing the diameter of the wire so that the resistance now is 50 ohms, gives a 1 mA-50 ohm movement which corresponds to a 50 mV. f.s.d. The 1 mA. 50 mV. meter will in some applications give a higher reading than, say, a 100 microamp. 1,000 ohm meter. Strange isn't it.

Whilst discussing the coil it should be mentioned that the coil former can be made to influence the meter characteristics. Nowadays aluminium is generally used and so arranged that it may or may not form a closed loop. The closed loop principle is used to dampen the movement of the coil, thus preventing overswing and oscillation of the pointer. Obviously this effect is caused by the well known "Eddy Current" phenomenon.

As the coil is normally wound with copper, its temperature co-efficient of resistance will be positive (p.t.c.). This would be of little consequence if the meter shunts were also of copper. However, this would be rather impractical. In past years coils were sometimes wound with copper to give a sensitivity of say 20 mV. f.s.d. and then the copper resistance "swamped" by adding a zero temp. co-efficient wire wound resistor to give an overall f.s.d. of 100 mV. Thus reducing the final t.c. to 20% of copper.

Modern practice uses a n.t.c. resistor (thermistor) and may be so arranged as to completely cancel out the p.t.c. of the copper coil.

THE SUSPENSION SYSTEM

The two most common types are:—

- (1) The pivot and bearing,
- (2) Taut band.

In the first type mentioned a hardened steel pin (pivot pin) is attached to the centre of the top and bottom horizontal of the coil. This assembly is then fitted into a housing containing jewelled bearings. These bearings may either be glass or sapphire (etc.), depending upon the ultimate meter quality required (a la watches).

Whilst the bearings are only tightened to a pressure of a few inch-pounds, the actual force applied to the pivot pins is quite considerable. This accounts for the seemingly high rate of wear in the cheaper class of meter.

A top and bottom coiled hair spring completes the above suspension system.

In the taut band system a fine flexible wire is attached to the coil where the pivot pin would normally be. These wires are then anchored and tensioned so that the coil is mounted in the desired position.

As the taut band contributes little in the way of friction, it is almost universally used in galvanometers and high class instruments.

In both systems the hair spring or torsion wire (taut band) perform the same functions:

- (1) Current connections to the coil.
- (2) Provides a counter force against which the rotational force acts.
- (3) Supplies the return force to reset the meter to zero.

THE INDICATOR

Many systems are used to provide the analogue readout from meters, the more common being:—

- (1) Pointer,
- (2) Light beam,
- (3) Vane.

The pointer is usually of a light non-ferrous material (aluminium, etc.) and may be either a spade end or knife edge configuration. The spade end type of pointer is normally used on the more robust and/or single scale meters, whilst the knife edge variety are used on the multi-scaled meter.

The use of a mirror reflector behind the pointer helps to eliminate the parallel error, and consequently is a standard feature on the better class of instrument.

Naturally a longer pointer produces greater resolution than a shorter one, hence it is wise to use the largest sized meter possible. However, a limit is reached when mechanical and weight problems make any further increase in size uneconomic.

The "light beam system" overcomes these problems and works as follows:— A small mirror, or prism, is attached to the coil system. A light source is beamed at it via a lens system and the reflection is focussed onto a scale some distance away.

In some very special applications, distance in the order of tens of feet are used. Where space is at a premium a second mirror is introduced, thus forming a reflex system. Sensitivities of 10 picroamperes per mm. for 1 metre throw are typical.

Vane type indicators are used for special applications such as industrial controllers, recorders, speedos, etc. The vane is usually a quadrant of light-weight material and is sometimes connected to the coil system via a gear arrangement. As this quadrant is moved it either covers or uncovers the activating system which may be air, light, magnetism or electrical.

COUNTER WEIGHTS

These are usually fitted to the lower end of the indicator and are used for balancing purposes. This feature enables the meter to be used in any position without impairing its accuracy

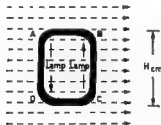


FIG. 1. ELEVATION VIEW.

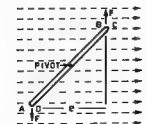


FIG. 2. PLAN VIEW.

unduly. Cushioned stops are used to prevent excessive overtravel.

Whilst the foregoing just about concludes the basic discussion on the principle of meter construction, a few further words are required covering usages.

THE CURRENT METER

The "D'Arsonval" meter may be used to measure such parameters as voltage, capacitance, inductance, etc. However, as it is basically a current operated device, my initial discussion will be on the ammeter.

Figs. 1 and 2 show the elevation and plan view, respectively, of a rectangular

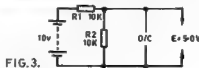


FIG. 3.

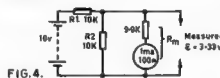


FIG. 4.

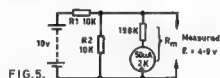


FIG. 5.

$$R_{\text{EXT}} = \frac{R_M}{(N - 1)}$$

where R_M is the meter resistance and N the desired extension factor.

Note the voltage drop across the combination will equal the mV. f.s.d. of the meter and hence provides one with an alternative method of calculating R_{EXT} .

$$\begin{aligned} \text{Total Load} &= R_1 + R_2 \\ &= 10K\Omega + 10K\Omega \\ &= 20K\Omega \\ \therefore I &= 0.5 \text{ mA.} \\ \therefore E R_1 &= 5.0V. \\ \text{and } E R_2 &= 5.0V. \end{aligned}$$

$$\begin{aligned} \text{Total Load} &= R_1 + \left(\frac{R_2 \times R_m}{R_2 + R_m} \right) \\ &= 10K\Omega + 5K\Omega \\ &= 15K\Omega \\ \therefore I \text{ will now} &= 0.666 \text{ mA.} \\ \therefore E R_1 &= 6.66V. \\ \text{and } E R_2 &= 3.33V. \\ \therefore \text{Error} &= 33\% \end{aligned}$$

$$\begin{aligned} \text{Total Load} &= R_1 + \left(\frac{R_2 \times R_m}{R_2 + R_m} \right) \\ &= 10K\Omega + 9.523K\Omega \\ &= 19.523K\Omega \\ \therefore I &= 0.51 \text{ mA.} \\ \therefore E R_1 &= 5.1V \\ \text{and } E R_2 &= 4.9V. \\ \therefore \text{Error} &= 2\% \end{aligned}$$

coil mounted vertically in a uniform magnetic flux field. The flux is horizontal and goes from left to right.

Suppose it has a strength of H lines per sq. cm., the coil N turns and the current through it I amperes.

In the vertical side of the coil there are N conductors of h cm. length carrying I amperes at 90° to the flux H lines per cm. square.

Therefore the force F on each side of the coil:

$$F \text{ (dynes)} = \frac{HNhI}{10}$$

The plan view shows the direction of these forces which form a couple. Now if e cm. is the distance between the lines of action, the torque will then be equal to Fe .

As H , N and h are fixed in the "force" formula, it may be re-written KI . It was stated earlier that the springs provide a counter force against which "F" acts to move the coil. This counter force is proportional to the deflection angle θ and the spring friction S . When the coil comes to rest the counter force:

$$\begin{aligned} S\theta &= KI \\ \therefore I &= \frac{S\theta}{K} \end{aligned}$$

Hence the deflection is proportional to the current and of course linear.

Meters are manufactured in a wide range of sensitivities and grades. It is usually more economical, in the long

The meter resistance may be ascertained by several means, some of which are listed:—

- (1) From technical specifications.
- (2) Direct measurement by bridge, ohmmeter, etc.
- (3) Substitution methods.

If using method 2, ensure that the test potential is such as to cause the meter under test to deflect backwards. This avoids the damaging mechanical shock when the pointer bangs hard over against the stop. The danger of burning out the coil is remote, particularly if the measurement is done quickly.

DIRECT VOLTMETER

The addition of a suitable series resistor enables the "D'Arsonval" meter to measure direct voltage. This resistor is selected so that when the desired full scale voltage is reached the total current through the combination is equal to the basic meter sensitivity. The series resistor is generally known as a range multiplier.

The meter, whilst still performing its original function of measuring current flow, is now calibrated in terms of voltage. The resistance required for a given f.s.d. is calculated using Ohm's Law

Suppose the meter movement is 1 mA. 100 mV. f.s.d. type and the re-

quired voltage range is 10.0 volts, then multiplier resistor

$$R = E \div I$$

$$= 10 \div 0.001$$

$$= 10,000 \text{ ohms}$$

Of course, for low voltage multipliers, the meter resistance should be subtracted otherwise an error will be introduced

When designing voltmeters for use over about 250 volts, it is wise to ensure that both the voltage and power ratings of the multiplier are not exceeded. Voltage co-efficients cause non linear scales whilst excessive power dissipation may permanently damage the resistor.

Sometimes it is easier to classify a metre as so many ohms per volt. The meter in the above example requires 10K Ω , hence 10K Ω \div 10v. = 1,000 ohms for each volt. Similarly, a meter of 50 μ A. would be 20,000 ohms per volt

A moving coil meter requires current for its operation, which of course must be supplied from the circuit under test. As a result, the voltage reading obtained is not correct and the error is caused by the added meter current flowing through the source impedance of the circuit under test. This effect may be reduced to a negligible level by using say a 50 μ A. (20,000 o.p.v.) meter rather than a 1 mA. (1,000 o.p.v.) type. See Figs. 3, 4 and 5.

ALTERNATING CURRENT

The basic movement may measure a.c. provided a suitable bridge rectifier is used with it. Because of threshold voltage and/or forward non linear resistance effects, it is not normal practice to use shunts when extending the alternating current ranges.

The current transformer, as shown in Fig. 6, is used to extend the basic range. It is possible, but not usual, to extend the range downwards, i.e. more sensitive.

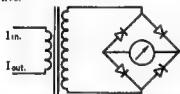


FIG. 6. CURRENT TRANSFORMER.

The current transformer may be made with a multitudinous number of turns ratios and is thus very useful. However it introduces problems of its own, such as poor frequency response, added circuit resistance, bulk, cost and worst of all, danger from the possible high voltage across the secondary if it becomes open circuit.

ALTERNATING VOLTAGE

Fig. 7 configuration is used to measure alternating voltage. However the D.C.I. through the meter is proportional to the average rather than the R.M.S. voltage. That is,

$$\text{D.C.I.} = \text{R.M.S.} \times 1.414 \times 0.636$$

$$= 0.9 \text{ R.M.S.}$$

Obviously the above result must be taken into account when calculating the multiplier resistance.

Example: Alternating voltage range desired, 0-1,000. Basic metre movement 0-1 mA.

$$\therefore \text{Multiplier } R = 1000 \times 0.9 \div 0.001$$

$$= 900,000 \text{ ohms.}$$

The above multiplier is 10% lower than that required for direct voltage. Hence for accurate work two sets of multipliers would be required if the same meter was to be used to measure both alternating and direct voltages.

A subterfuge which the author uses is to shunt the meter, on direct voltage, so that the f.s.d. requirement is raised by 10%. On alternating voltage the shunt is switched out of circuit, thus enabling the same multiplier to be used for both conditions.

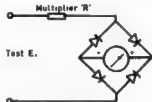


FIG. 7. ALTERNATING VOLTAGE.

All of the above assumes that sine waves only are being measured. If steady tone signals (square, triangular waves, etc.) are to be measured then the values of 1.414 and 0.636 would have to be changed accordingly.

As the average and R.M.S. values are constantly changing in speech and music, it should be obvious that moving coil plus rectifier instruments are not really suitable for the measurements of this type.

One final word, note that on low voltages threshold and rectifier voltage

drop effects interfere with the scale accuracy and linearity, etc.

Well chaps, that about wraps it up for now. I hope you found the article interesting enough even though most of the information presented was rather basic. However, basics are often overlooked, resulting in misleading measurements and thus false conclusions.

★

Book Review

RADIO AMATEUR'S HANDBOOK

It's that time of the year again. The time to review yet another edition of the book commonly known as the A.R.R.L. Handbook. This time it is the forty-seventh edition of the book which has been published continuously since 1928 and has distributed more than four million copies. But now for the big question: Is this edition of the handbook worth buying?

If you are a newcomer to Amateur Radio, or are even slightly interested, and you do not have a recent copy of this handbook, read no further! Just go straight out and buy a copy. It does not cover everything pertaining to Amateur Radio and it does not always cover those items included in the fullest detail, but it comes closer to doing so than any other book available at a reasonable price. For those of you whose copy is a few years old, you also should buy this issue.

Considerable revision has taken place in both the theory and construction sections and experimenters will be delighted not only at the increased coverage of the theory side of semiconductor electronics, but also at the very large increase in the number of solid state construction projects both h.f. and v.h.f. And, of course, the greatly expanded tables of the latest transistor and diode specifications.

The Portable/Mobile and Antenna chapters have been completely re-written and updated. For the first time treatment has been given to v.h.f. repeater stations and to satellite communications. All in all, a very good edition of the A.R.R.L. Handbook to have in your bookcase or workshop. The only major criticism would be one that unfortunately applies to most publications from the U.S.A. and that is the use of many components in the construction projects which are described by little more than their catalogue numbers, which, needless to say, do not apply in Australia.

Published by the American Radio Relay League. Review copy supplied by the A.R.R.L. Available from the W.I.A. P.E. Publications Department, P.O. Box 67, East Melbourne, Vic. 3002. Price \$3.95.

RADIO MECHANICS

(FOR PORT OF SYDNEY)

THE MARITIME SERVICES BOARD OF N.S.W.

QUALIFICATIONS: Applicants must be qualified tradesmen with experience in modern transmitters/receivers and be capable of assisting in the development of specialised equipment including the construction and modification of prototype models. The successful applicant will also be engaged on installation maintenance and testing of radio equipment and electronic navigation aids. Solid State Circuitry experience is a necessity.

WAGE \$69.95 per week. Fares over \$1.00 and other allowances

CONDITIONS: Sydney based; four weeks annual leave. Applicants must be prepared to work overtime if required. Occasional call outs to the North and South Coast are covered by appropriate allowances.

Particulars and interview:

SENIOR ELECTRICAL ENGINEER, Phone 2-0545 Ext. 422 office hours

H. B. CADELL, Secretary.

Construction of Low Loss Co-axial Cable

H. N. SANDFORD,* VK4ZT

It is convenient to use rigid co-axial cable to support feeds in parabolas used on 1296 MHz. and higher

THE difficulty and expense in obtaining suitable low loss co-axial cable prompted the investigation into methods of construction using locally available materials. It was found uneconomical to purchase short lengths of rigid co-ax. as the cost of the associated connectors would be several times that of the cable alone. For example, a 20 ft. length of 7/8" diameter rigid co-ax. is about \$70 and fitted with flanges both ends \$80. Flanged adaptors with type N connectors are about \$27 each, so the total cost of a 20 ft. length with type N connectors would be about \$144 or just over double that of a standard length of co-ax. alone. These figures were taken from an American catalogue and, of course, are for high quality components suitable for use to 3 GHz. As a matter of interest, the attenuation of this co-ax. at 1300 MHz. is about 1.6 dB/100 ft. rising to about 3 dB/100 ft. at 3.3 GHz.

COPPER CO-AX. CONSTRUCTION

The first method investigated employed copper pipe available from plumbing suppliers. At the time I could only obtain 3/4" o.d. x 20 gauge and 1/4" o.d. x 20 gauge tubing for the inner conductor. The theoretical impedances and cost (these will only be an indication due to fluctuation in copper prices) for a few combinations are as follows:—

Outer I.D.	Inner O.D.	Z ₀	SWR	Approx. Cost per ft.
1" x 20g.	1/4" x 20g.	59.5	1.18	70c
1" x 20g.	5/16" x 20g.	46.2	1.08	75c
3/4" x 18g.	1/4" x 20g.	55.8	1.15	85c
3/4" x 18g.	5/16" x 20g.	54.0	1.08	\$1.03
	20g. —	0.678"		
	18g. —	0.654"		
	16g. —	0.627"		

All of the above a.w.r.'s were acceptable for the project as the mismatch loss would be negligible. Various methods may be used to cope with the mismatches or the system could be designed around the nominal impedances. In any case, much of the cheaper flexible solid dielectric co-ax. cable available is no better than this. Type N female connectors were fitted at each end. The cheapest method found was to use a type N female to female connector (UG29B/U, commonly referred to as a "bullet"), cutting the connector in half to provide a transition at each end of the co-ax. It also provides a convenient support for the inner conductor. See Fig. 1.

Carefully cut the body of the connector in two places 1/8" either side

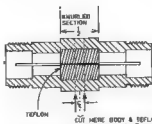


Fig. 1—UG29B/U Type N Connector showing the position of cuts to make two end adaptors

of the centre so as to remove 1" from the body. Withdraw the inner conductor and cut exactly in half. The Teflon insert may now be cut off flush with body so when the inner pin is refitted there will be 1/8" protruding from each cut portion of the connector. If a lathe is available, the outer may be parted off.

Prepare the inner copper tubing conductor of the co-ax. by cutting 1" shorter than the desired length of the outer 3/4" pipe. Plug the ends of the inner tube with a neat fitting piece of brass or the shoulders may be filed off a small brass nut. Solder the plug into



Fig. 2—Assembly of Type N Connector to Copper Co-ax

the ends of the tube and drill out for a neat fit on the centre pin of the connector.

Teflon washers are fitted on the inner conductor at 3 to 5 ft. intervals to support the inner conductor centrally. These may be cut from 1/16" Teflon sheet. The sheet is available from Bearing Suppliers and is very expensive, but the small amount required should cost less than \$1. Polystyrene or Polythene would also be suitable.

Teflon or Polythene is best cut using a short piece of either tubing. With a pair of dividers, lightly scribe two circles with diameters of the o.d. of the inner and the i.d. of the outer. File or turn about a 60° angle on the outer end of the 3/4" tube to make a sharp edge on the inside circumference. With the 1/4" tube, run a 3/8" drill into the end until a sharp edge is produced on the outside circumference. Place the Teflon or Polythene on a smooth hard piece of wood. The washer may now be cut with a sharp blow using the two

tubes as cutters. Polystyrene will, of course, require drilling and cutting.

Slide the spacers onto the inner conductor at the desired spacing. If care is taken, these will be a tight fit on the inner. The outer edge of the spacers should now be filed down slightly so as to slide neatly inside the outer tube without binding.

The two pins should now be soldered into the ends of the inner conductor, taking care to fit the Teflon spacer from the connector beforehand.

The inner surface of the outer tube should be tinned for approximately 1/4" in at each end. Solder the body portion with approximately 1/8" of the connector extending into one end of the outer tube. Depending on the gauge of the outer tube, it may be necessary to fit a 1/8" wide strip of shim brass between the body of the connector and the tube, before soldering. 18 gauge tube should provide a neat fit.

Slide the inner conductor carefully into the outer conductor, taking care not to move the spacers. Push right home so the Teflon spacer and pin fit correctly into the end socket already fitted. The other connector body is finally soldered into position, completing the assembly of the co-ax. Use only

sufficient heat to solder, and it is a wise precaution to tilt the end being soldered down slightly to prevent any solder running back into the co-ax. The complete assembly is shown in Fig. 2.

PERFORMANCE

The reflection co-efficient of a 6 ft. length of this co-ax. was measured using a Hewlett-Packard 1415A Time Domain Reflectometer. The characteristic impedance was measured at 57.5 ohms, which is slightly lower than calculated and may be due to tolerances of the tubing used. This gives an a.w.r. of 1.15. A copy of the TDR trace is shown in Fig. 3.

The two pronounced dips are due to the capacitive reactance of the two Teflon spacers but only amount to a reflection co-efficient of approximately 2%. It is possible to compensate by cutting a groove in the inner conductor, but in view of the small reflection obtained, this was considered unnecessary.

* 18 Loch Street, Trowaamba, Qld., 4350.

sary. The irregularities in the line are no worse than those observed on a piece of good quality flexible co-ax. The TDR response extends to 2.3 GHz., so this method of construction is probably suitable for narrow band work to at least 3.3 GHz and possibly higher. Attempts to measure the loss were unsuccessful as this appeared to be less than 0.1 dB. at 1296 MHz.



Fig. 3—TDR Response of Copper Line with Type N Connectors.

ALUMINIUM CO-AX. CONSTRUCTION

Tom Norris,† VK4NO, used aluminium tubing and BNC connectors on a similar project. The outer tube consisted of 1" o.d. x 18g., and the inner 3/8" o.d. x 18g. Tapered sections were machined to match the co-ax. dimensions to the BNC connectors. The calculated impedance of this line is 52.5 ohms and the measured impedance using the TDR was 52.8 ohms. The nominal dimensions of the tubing were within 0.001".

Slightly different techniques are required due to the connectors and materials used.



Fig. 4—Assembly of BNC Flange Mounting Connector to Aluminium Tube

BNC FLANGED CHASSIS MOUNTING CONNECTOR

Refer to Fig. 4 for details of this construction. A slight modification is required to one connector to allow for easier assembly. This involves removing the swaging that retains the Teflon and centre pin.

The outer block is made of aluminium 1" long and turned to fit neatly in the outer tube. The inner hole is arranged to fit over the Teflon at the rear of the connector. This will depend on the particular connector used. The inside taper is linear from this hole that fits the connector to nothing at the inner diameter of the outside tube. The inner tapered section is made of brass and the starting diameter of the inner at the rear of the connector may be calculated from the normal formula, $Z_c = 138 \log (D + d)$, which for 50 ohm co-ax transposes to

$$d = 0.4409 \times D$$

where D = i.d. of the outer,
 d = o.d. of the inner,
and Z_c is the characteristic impedance.

Taper the inner section from this calculated value up to the o.d. of the inner aluminium conductor. A neat hole is bored to fit the BNC pin. The other end is turned to be a neat fit in the inner conductor. The brass section may be tapered to reduce the possibility of electrolytic action. If desired, the tapered section may be a heat shrink fit in the inner, or may be pinned. Assembly is straight-forward.

Fit the tapered sections to the inner conductor after determining the correct length. Solder the pin and Teflon from the modified connector to one end of the inner. Fit one of the outer tapered blocks into one end of outer tube. Slide the inner into the outer tube so the inner protrudes through the end block. Solder the unmodified connector to this end of the inner, then mount the connector flange with fixing screws tapped into the block. The other end block may now be fitted. Finally, the body of the remaining connector is screwed into place. If desired, both connectors may be modified to remove the inner pin and Teflon block for easier fitting.

BNC THREADED CHASSIS MOUNTING CONNECTOR

A suggested method of mounting is shown in Fig. 5. The outer tapered aluminium block and the inner tapered brass section is of the same construction as detailed in the preceding section.

Both connectors are modified by removing the swaged retaining section to allow removal of the centre pin and Teflon block for ease of assembly.

The connector may be mounted with an adaptor block tapped to take the connector (3/8" x 32 threads per inch). The normal mounting nut may be used as a locking nut. The adaptor block is attached to the outer aluminium tapered block with tapped mounting screws.

An alternative method would be to solder the mounting nut to a piece of,

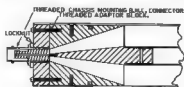


Fig. 5—Assembly of BNC Threaded Chassis Mounting Connector

(Other details and dimensions as Fig. 4.)

say, 16 gauge brass plate, and screw this to the outer aluminium tapered block—in effect, converting the connector to a flange mounting or, if desired, the connector body could be soldered directly to the plate. The cost of 1 ft. of this co-ax. is in the order of 34 cents.

PERFORMANCE

A copy of the TDR trace of a 6 ft length of aluminium co-ax. is shown in Fig. 6. The Teflon spacers are evident and the larger transition steps at each end are caused by the BNC connectors which are not as good at these frequencies as the type N connectors. Some of the discontinuity, however, was introduced by the BNC to type N adaptors used at either end for measurement.

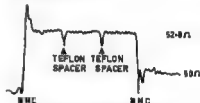


Fig. 6—TDR Response of Aluminium Line with BNC Connectors

In any case, the steps due to the connectors do not exceed 3 to 4%, and should be satisfactory for use to several GHz. The loss was too low to measure with methods available, being less than 0.1 dB. The measured impedance of 52.8 ohms gives an SWR of 1.058.

WEATHERPROOFING

The copper co-ax. should be suitable for outside use, as it is completely sealed by the waterproof type N connectors.

The cheaper aluminium co-ax. would be more difficult to seal, but probably could be done by sealing the joints with suitable paint. A better method would be to fit O-rings in grooves around the outer tapered block. It would only then be necessary to seal the connector to the block with paint. Alternatively, dry air may be blown into the co-ax. under a slight pressure and allowed to leak out around the joints, thus preventing the ingress of moisture.

JOINING LONG LENGTHS

It is a relatively simple matter to join 18 ft. or 20 ft. stock lengths of tube to produce long low-loss runs. A neat fitting inner plug similar to the end of the inner tapered section can be used to join the inner conductor. The outer copper tube may be joined by sweating a neat fitting outer tube over the butt joint. The aluminium outer presents a more difficult problem, but could be joined using a neat fitting sleeve locked in place with lock screws tapped into the sleeve. An O-ring in a groove at each end of the sleeve could be used to provide weather proofing or possibly a smear of "Araldite" or similar adhesive at each end of the sleeve would be satisfactory.

(Continued on Page 15)

THE EFFECTIVE VALUE OF AN ALTERNATING CURRENT

LECTURE NO. 5

C. A. CULLINAN,* VK3AXU

Some knowledge of Calculus is desirable for this Lecture

A direct current (d.c.) of electricity is a steady current travelling with time in one direction only, i.e. it is either Positive or Negative and remains such until some action is taken to alter its value or stop it entirely.

An alternating current (a.c.) of electricity is not steady but continually rises, falls and reverses itself, twice becoming zero and twice rising to a maximum, but in opposite directions in one complete cycle of changes.

In a simple alternating current generator, termed an alternator, let us assume that we have two magnets arranged opposite each other, one North and one South with a single loop of wire arranged so that it can be rotated between them.

Also, let us assume for a moment that the two magnets are vertical and that the loop of wire is horizontal.

Let us connect a centre zero ammeter in series with the loop of wire, then start to rotate the loop in a clock-wise direction.

Due to the phenomenon of Induction it will be found that as the loop approaches each of the magnets as it turns 90°, then the ammeter will show that an electric current is flowing in the loop. This will reach a maximum when the loop has turned 90°, i.e. its plane is in the same plane as that of the magnets.

However, as the loop is rotated further the current flowing in the ammeter will decrease and become zero when the loop is at 180°.

Now as the loop continues to rotate the current in the ammeter will be seen to rise, but in the opposite direction until a maximum is reached at 270°. With further rotation the current will fall and zero is reached at 360°. Thus the current twice becomes zero at 0/360° and 180°, and twice becomes a maximum (of opposite polarity) at 90° and 270°. One complete rotation is known as one cycle. The loop of wire is known as an armature. If the armature is rotated at 3,000 revolutions per minute, then it will rotate 50 times each second. $3,000 \div 60 = 50$.

Therefore we would say that the number of cycles per second is 50. This is known as the frequency of the alternating current.

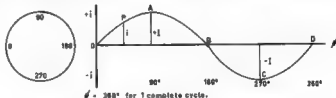
If speed is 3,600 r.p.m. then the frequency is 60 cycles per second, or if speed is 6,000 r.p.m. then the frequency is 100 cycles per second.

From this it will be seen that the frequency of an alternating current is the number of cycles which occur in each second of time.

If the armature is rotated quickly the zero centre ammeter will not be able to follow the rapid alternations of current and its use in this explanation is more hypothetical than practical.

Continuing the series of lectures by C. A. Cullinan, VK3AXU, at Broadcast Station 3CS for students studying for a P.M.G. Radio Operator's Certificate.

It must be realised that the loop of wire can only be rotated during a finite period of time. If it ceases rotation then there cannot be any current flow as the property of induction will cease too. In our simple alternator the magnets may be permanent magnets or electro-magnets having a constant magnetic field produced by supplying the electro-magnets with Direct Current. Also no matter how fast the loop is rotated it must take some amount of time to complete one revolution or cycle. In actual practice there are limits to the maximum speed of rotation that can be achieved.



Because of the time taken to make each revolution, the maximum current in one direction, say positive, is then followed by the maximum current in the opposite direction, but because of the time difference between the two maxima neither will cancel the other.

Thus it becomes possible to display the rotation of a single cycle of the loop or armature as a circle

Now this circle can be transferred into a graph, having time shown horizontally and the amplitude of the current shown vertically and the resulting curve will be the well known Sine curve, i.e. let us roll the circle along a straight line and plot the resulting curve (see above diagram).

We desire to find the "effective" or equivalent steady current when the maximum value of one cycle is known.

In an a.c. circuit the power is not proportional to the current itself (since this varies as can be seen from the sine curve), but to the square of the current flowing in a resistance R.

Thus Power = Ri^2 .

Let I be the maximum value of current for the cycle and i the instantaneous value at any time t , and f the frequency in cycles per second.

Then i is given by the formula:

$$i = I \sin (2 \pi f t)$$

where $(2 \pi f t)$ is the phase angle of the cycle and is known as θ ,

therefore $i = I \sin \theta$.

In one complete cycle $\theta = 360^\circ$ and the graph of this equation is shown in Fig. 1.

The curve O A B C D is repeated for each individual cycle and I is the height of the maximum current. The ordinate at any point can be shown as P and the instantaneous current corresponding to any phase θ is i .

It will be seen that the loop O A B is exactly equal in shape but opposite to the loop B C D, therefore the current generates exactly the same amount of power in the positive half of the cycle as it does in the negative half.

Therefore the effective current is the same for each half of the cycle, thus the same for each complete cycle as long as the current continues to flow.

Let us then calculate the effective value of the current for the half cycle O A B.

As mentioned before, at any instant when the phase is θ , then the current is i as shown at P.

We have already said that Power = Ri^2 , also that $i = I \sin \theta$. Therefore the power generated per second of time = Ri^2 .

$$= R (I \sin \theta)^2$$

$$= RI^2 \sin^2 \theta$$

The average value of this power for all values of θ over the entire cycle of 360° is the same as would be generated by the equivalent or effective current, where I_e represents the equivalent or effective current, then the power generated by it is $R I_e^2$ and this must be equal to the average of $R I^2 \sin^2 \theta$ over the cycle or half cycle.

In order to find the average value of any quantity over a certain range we integrate it over that range (or sum up all its values over that range) and divide by the total range.

Now the Integral (or sum) over half a cycle (0-180°) = 0 to π , is

$$\int_0^\pi$$

and therefore the average as stated above is

$$\frac{\int_0^\pi}{\pi}$$

* 6 Adrian Street, Colins, Vic., 3205.

The average of this expression for the varying phase is therefore,

$$\frac{1}{\pi} \int_0^{\pi} (R I^2 \sin^2 \theta) d\theta$$

The $d\theta$ means the difference or differential or part of the angle θ , and as $R = I$ are constants, this becomes,

$$\frac{R I^2}{\pi} \int_0^{\pi} \sin^2 \theta d\theta$$

as stated previously, this is equal to $R I^2$, hence,

$$R I^2 = \frac{R I^2}{\pi} \int_0^{\pi} \sin^2 \theta d\theta$$

Divide by R

$$I^2 = \frac{I^2}{\pi} \int_0^{\pi} \sin^2 \theta d\theta,$$

and to determine the value of the effective current I_e , we must integrate $I^2 \sin^2 \theta d\theta$.

To do this we use the trigonometrical relationship $\cos^2 \theta = 1 - 2 \sin^2 \theta$.

Therefore $\sin^2 \theta = \frac{1}{2} (1 - \cos 2 \theta)$ therefore $\int \sin^2 \theta d\theta$

$$\begin{aligned} &= \frac{1}{2} \int (1 - \cos 2 \theta) d\theta \\ &= \frac{1}{2} \int d\theta - \frac{1}{2} \int \cos 2 \theta d\theta \\ &= \frac{1}{2} \theta - \frac{1}{2} \int \cos 2 \theta d\theta \end{aligned}$$

$$\begin{aligned} \text{Now } \frac{1}{2} \int \cos 2 \theta d\theta &= \frac{1}{2} \int 2 \cos 2 \theta d\theta \\ &= \frac{1}{2} \int \cos 2 \theta \cdot 2 d\theta \\ &= \frac{1}{2} \int \cos 2 \theta \cdot d(2\theta) = \frac{1}{2} \sin 2 \theta \end{aligned}$$

$$\begin{aligned} \text{Hence } \int \sin^2 \theta d\theta &= \frac{1}{2} \theta - \frac{1}{2} \sin 2 \theta \\ &= \frac{1}{2} (\theta - \sin 2 \theta). \end{aligned}$$

Remember earlier we showed that

$$I_e^2 = \frac{I^2}{\pi} \int_0^{\pi} \sin^2 \theta d\theta$$

$$\begin{aligned} \text{therefore } I_e^2 &= \frac{I^2}{2\pi} \left[\theta - \frac{1}{2} \sin 2 \theta \right]_0^{\pi} \\ &= \frac{I^2}{2\pi} \left[\left(\pi - \frac{1}{2} \sin 2\pi \right) - \left(0 - \frac{1}{2} \sin 0 \right) \right] \\ &= \frac{I^2}{2\pi} = \left(\pi - \frac{1}{2} \sin 360^\circ \right) \\ &= \frac{I^2}{2\pi} (\pi) \end{aligned}$$

$$\text{therefore } I_e^2 = \frac{I^2}{2}$$

$$\text{therefore } I_e = \frac{I}{\sqrt{2}} = 0.707 I.$$

Thus the effective value of an alternating current is 0.707 of the maximum current.

Similarly the effective voltage in an a.c. current $E_e = 0.707 E$, where E is the maximum voltage in the cycle.

Ordinary a.c. voltmeters and ammeters indicate the effective value. (There are special meters which read the peak value.)

Thus when reading the voltage or current in an a.c. circuit it must be remembered that this will be the effective value (except where the peak reading meters are used).

Therefore if the effective or average value is known, the peak voltage or current can be calculated readily.

$$I_e \text{ or } E_e = 0.707 I \text{ or } E$$

$$\text{therefore Peak value} = I \div 0.707 = 1.41 I.$$

The discussion above has assumed that the a.c. current is the same for both halves of the cycle.

However, this is not true with audio-frequency currents and voltages as found in music and speech.

Therefore the Australian Broadcasting Control Board implies, by regulation, that the difference between the average power as read by a Vu meter and the peak power will be 8 decibels.

Thus in Australia this figure must be used, although other countries may use a different value.

Vu meters used in studios and on professional tape recorders read the average or effective value, whereas the peak reading meters used on some recorders read the peak value. This must be remembered when testing such machines.

When testing a tape recorder with a sine wave, or a broadcasting system, it is necessary to test at normal level and at 8 decibels above this.

In a transmitter the maximum level is that which produces 100% modulation of a sine wave, referred to 1,000

cycles per second. Then the average value of a test signal is set 8 db. below this figure, i.e. 40% modulation.

When dealing with a.c. power systems, a.c. motors and the like, it should be remembered that voltages are quoted on the average figure.

Insulation, valve and solid state devices must be considered in the light of the peak value plus a margin for safety.

Thus a power transformer designed to give 300 volts a.c. each side of a centre-tap, will give 300 volts average or 800 volts across the whole winding. However, the peak or maximum voltage will be $800 \times 1.41 = 848$ volts.

PROVISIONAL SUNSPOT NUMBERS

APRIL 1970

Dependent on observations at Zurich Observatory and its stations in Locarno and Arosa.

Day	R	Day	R
1	115	16	92
2	96	17	92
3	133	18	69
4	116	19	87
5	120	20	85
6	118	21	64
7	123	22	87
8	147	23	97
9	172	24	90
10	188	25	93
11	183	26	81
12	193	27	88
13	161	28	100
14	184	29	112
15	168	30	116

Mean equals 109.1.

—Swiss Federal Observatory, Zurich.

Construction of Low Loss Co-axial Cable

(Continued from Page 13)

A more complex locking arrangement using a gland at each end could also be devised, but would require considerable machining.

RELATIVE COSTS

These are estimated for 18 ft. lengths and provided only as a guide (Table 1).

An allowance has been made for miscellaneous items, Teflon, etc. It will be seen that aluminium construction is the cheaper, unfortunately involving more effort.

CONCLUSION

It has been shown that satisfactory low-loss rigid co-axial cable can be

manufactured at relatively low cost. Whilst the initial cost of the copper co-ax. is higher, only hand tools are required in the construction and is suitable for all weather use. The aluminium co-ax. construction is cheaper and lighter, but more complex, requiring the use of a small lathe and is also more difficult to weatherproof.

It has also been demonstrated that measured values agree closely with calculated values, thus allowing the design to proceed with confidence, especially when measuring equipment is not available.

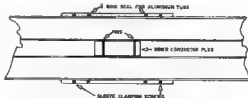


Fig. 7.—Joint for Aluminium Co-ax. For Copper, inner and outer may be swaged.

Material	Outer	Inner	Cost/ft.	Connector Cost	Zc	Total Cost
Copper	3/4" x 20g.	1/4" x 20g.	70c	Type N \$2.50	56 ohms	\$16.00
Copper	3/4" x 16g.	1/4" x 20g.	\$1.03	Type N \$2.50	54 ohms	\$22.00
Aluminium	1" x 18g.	3/8" x 18g.	34c	BNC \$2.25	53 ohms	\$9.00

Table 1.—Estimated cost for 18 ft. lengths of co-ax.

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"Where Have All Those Good Hams Gone?"

Not a bad question, not such an uncommon one. Especially if you live in certain areas of our VK4 land. Why don't you hear as much of old pro's such as Mick VK4ZAA, Dane VK4ZAX or Tom VK4ZAL, just to think of a few, I have no doubt much the same is asked of many Amateurs in VK3 land.

The answer is simply given, but not as easily understood. The answer—Channel 6.

We, in many areas, particularly VK3 and VK4, certainly know why we are not heard of so often these days. But can any of us give a good sound reason why this has come about.

The practical explanation is simple. Suddenly you have a transmitter only 250 kilocycles away from the bottom of your band. Effective radiated power: 100 kilowatts vision, 20 kilowatts sound. Bad enough, even discouraging!

But combine the complex, varying pulse nature of the vestigial video modulation with a frequency modulated intercarrier, and the result just has to be heard to be believed.

So we tried filters, we tried low cross-modulation converters, we tried a lot. And results were sometimes good. However, it was not good for long. Old t.v. himself soon showed. Back to the old drawing board. High pass filters, 52 megacycle oscillators, shielding and just about everything else too! But those t.v. sets just don't cut off response at 52 megacycles.

So "t.v. reigns, even though transmissions are clean, stable, and in most cases, on quite low power. Officially the verdict is, and we must abide by it, NO 6 metre transmission during Channel 6 programming.

This gives us no evening transmissions at all, unless, at least, after 2300 E.A.S.T. Mornings are available week days and Saturdays to 0900 or so, and Sunday, if lucky, to 1100 hours.

As mentioned earlier, this answers "why" to some questions, but what is the reason.

Possibly one reason is that most of us, myself included, did not realise just how bad things were going to be, when that 2 megacycles of our 6 metre band slipped away.

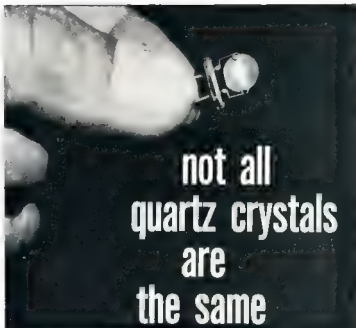
Another reason, certainly, must be the disappointing lack of consideration which must have been shown towards our Amateur Services, of present and past, by persons in control of frequency allocation.

But whatever the reason, the damage is done. "Fifty to Fifty-two" is gone for good. So have a lot of the old 6 metre Amateurs. Whether we can place any blame on ourselves or others for allowing these circumstances to arise is not at question anymore. It is too late.

But, please chaps, never let it happen again. Once part of any Amateur band is gone, it is gone for good.

And, sadly enough, on 6 metres, a lot more than 2 megacycles have gone. So have too many good friendships which we looked forward to renewing every DX season.

—J. D. Bisgrove, VK4ZJB/T.



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OSCAR 6—THE AUSTRALIAN "BIT"

LES JENKINS,* VK3ZBJ

The OSCAR 6 satellite will, it is hoped, be launched into orbit about the middle of next year. The orbit path will probably be similar to that followed by AUSTRALIS OSCAR 5, a near-polar orbit at a height of about 1,000 miles. This would allow Amateurs in Japan to contact their fellows in eastern Australia and would make trans-Tasman Amateur communications on v.h.f. a regular and reliable fact. Similarly, trans-Atlantic contacts on v.h.f. will become almost routine.

OSCAR 6 will carry two independent communications systems; transponder A (built in Australia) and transponder B (built in Germany). The two transponders are completely different in their operation, so it is important that intending users become acquainted with their operation and with the equipment that will be required to use them. The following description of the VK portion of the payload will enable intending users to prepare themselves well in advance of the launch, so that maximum use may be made of the satellite.

SYSTEM OUTLINE

The basic concept is that of a repeater system. Signals are received by the satellite in the 2 metre band, demodulated and the recovered audio used to modulate the downlink transmitter, which radiates in the 75 cm. band. Several channels are available, each with its own separate receiver i.f. system and transmitter. The inputs for the i.f. amplifiers are derived from a common primary converter.

As the incoming signal is demodulated, it will be obvious that only one mode can be accommodated. The one chosen is f.m., with the specifications being compatible with currently used f.m. "Carphone" type equipment.

Two other sub-systems will be provided—a multi-channel digital command system and a multi-channel telemetry system. These will be shared by all systems on board the spacecraft and will enable either communications transponder to be activated alternately, as well as providing for corrective measures to be exercised in the event of failure of certain spacecraft functions.

The telemetry system will provide some 60 channels, shared by both transponders, the output of which will be r.t.t.y. This will be compatible with normal 850 Hz. shift, 45.5 Baud systems. The downlink frequency for the telemetry, as well as the modulation mode, will depend on which transponder is activated.

CHOICE OF INPUT-OUTPUT BANDS

Some readers may question the choice of input-output frequencies. The choice is based on the following considerations:

1. **Elimination of Mutual Interference** If the uplink band is 75 cm., then the output from the downlink in the 2 metre band would have harmonics falling in the bandpass of the receiver

input circuits. Even if these are well down in amplitude, say, —50 dB, they are still quite large signals and may produce undesirable responses and "birdies" in the receiver system. More importantly, they can de-sensitise the receiver, thus requiring more ground station power to acquire the satellite.

It may be argued that these faults can be rectified by the use of suitable filters and choice of frequencies. However, it seems an unnecessary hardship to impose on the satellite builder if a simpler solution is available.

The case of the wholly "inband" system (i.e. 2 metre/2 metre, or 75 cm./75 cm.) is discarded for the above reasons, and this is supported by experience with ground-based systems. Such operation in the 75 cm. bands is feasible. However, this band is restricted in certain geographical regions and this, on a world basis, poses some problems.

The 2 metre input/75 cm. output system has several advantages. In the first place, it is possible to generate 432 MHz output without producing spurious signals in the 2 metre band. This is accomplished in the VK system by generating at 13.5 MHz, and "doubling all the way". The resulting system allows antenna configurations and sub-system layouts within the satellite to be arranged without regard to input-output coupling.

This coupling between antennae on a small spacecraft is extremely tight if antennae for the same band are used.

AO5, for instance, suffered extreme crosstalk between the input and output antennae; so much so, that 10 kW. e.r.p. was required to exercise command! The demonstration model of OSCAR 6 has its antennae intermingled, with no measurable degradation in receiver sensitivity.

2. **Ground Equipment.** From the user's point of view, the ground equipment requirement is the most important aspect of satellite operations. In this respect there is not much difference between systems, with "inband" techniques requiring only one antenna being the most favorable. The most effective use of power, both on the ground and in the spacecraft, favors 75 cm. for the uplink and 2 metres for the downlink. High gain antennae for 75 cm. are small and easily mounted and the larger capture area of 2 metre antennae requires less downlink power for the same result. The higher path loss on 75 cm. is more easily made up with both higher power output and high gain antennae on the ground, whilst lower path loss on 2 metres means less transmitter power required in the satellite.

This argument is certainly in favor of the opposite system. However, when the ground requirements are presented the reader will see that things are not quite so bad after all. Those who tracked AO5 will remember how good a signal they received, and this from 100 mW. of output power. It follows that 100 mW. on the ground into a

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receiving antenna would reach the satellite just as well. If a standard f.m. mobile unit with, say, 10 watts of carrier output is used, then the signal into the satellite will be 20 dB. higher than the signal received from AOS. When one takes into account the fact that the receiver in the satellite is an f.m. unit, it follows that a very solid, noise-free signal can be put into it for a very small amount of power on the ground. Let us do some simple arithmetic and see what this all means in terms of output power.

The satellite receivers have the following characteristics:—

Input frequency: 144–146 MHz.

I.f. bandwidth (—40 dB.): 50 KHz.

Input noise figure: 0.8 dB.

6 dB. quieting: 0.07 microvolt (50 ohm).

20 dB. quieting: 0.18 microvolt (—124 dB.).

To a first approximation, we can calculate the path loss as:—

$$L = 37 + 20 \log F + 20 \log D$$

where F is frequency in MHz.

D is distance in miles.

If we put $F = 150$ MHz.

$D = 2,000$ miles,

then $L = 37 + 87 + 68$ dB.

$= 153$ dB.

Assuming a radiated power of 1 watt or +30 dbm., then the signal at the input to the receiver = +30 — 153, or —123 dbm.

This, of course, takes no account of antenna gains, feeder losses, etc., and assumes best case for antenna coupling between ground and satellite. However, it is clear that 1 watt will give something like 20 dB. of quieting in the satellite receiver. An increase of 20 dB., i.e. 10 watts into a 10 dB. gain antenna, would increase this input to almost 2 microvolts, which gives full quieting in the receivers and then some! In fact, mobile stations should be able to put an adequate signal up to the satellite. However, they may have some difficulty in hearing the downlink and this brings up the question of receiving equipment.

Before discussing the ground requirements for receiving the 75 cm. downlink transmissions, a few words on the satellite transmitters would be in order. The transmitters consist of a frequency modulated crystal oscillator at 13.5 MHz., multiplying up to 216 MHz. at a power level of 1.5 watts. This is passed to a varactor doubler, producing 1 watt output at 432 MHz. Assuming that a total of five channels are used, including the telemetry downlink, this requires a total output of 5 watts which, at an overall efficiency of 33% d.c. to r.f., means a d.c. input power of 15 watts is required for the transmitters only. As only 6 watts of charging power is available from the satellite's solar cells, this seriously limits the operating time of the system. However, as the transmitters draw no current in the absence of an input signal, the duty cycle will depend on the number of stations using the satellite during an orbit. As much of the time the satellite will be over areas of the world where there are no stations active, the situation is not quite so bad as first appears.

Assuming all the power generated is radiated, then one can calculate the

received signal as for the uplink, plugging in the values for 432 MHz.

This gives:—

$$L = 37 + 20 \log F + 20 \log D$$

$$= 37 + 66 + 52.7$$

$$= 155.7$$

$$= \text{approximately } 156 \text{ dB.}$$

If 1 watt = +30 dbm.

$$\text{then } Pr = +30 - 156 = -126 \text{ dbm.}$$

This corresponds to about 0.1 microvolt in 50 ohms at the terminals of a dipole, assuming the dipole to have unity gain. If a low noise (3–4 dB.) mast head amplifier is used, then an input of 0.1 microvolt will result. It is emphasised that these figures are a first approximation only and are best case. However, if an antenna gain of 10 dB. is available, this will boost the input to 0.7 microvolt, which should make a reasonable impression on a good quality f.m. receiver. It is unfortunate that high gain antennae yield narrow beamwidths, as this requires the antenna to track the satellite at all times. The higher the gain, the more accurate tracking must be.

Summarising these results, it is evident that the receiving requirements far outweigh the transmitting side.

However, on the credit side, being an f.m. system, the capture threshold

is quite well defined, and once the signal exceeds this value, then the S/N ratio climbs rapidly.

Up to this point, nothing has been mentioned about Doppler shift on the signals. The uplink on 2 metres will have a maximum excursion of approximately 8 KHz. An a.f.c. loop in the receivers will automatically correct for this for each channel, providing the input signal is within 10 KHz. of the nominal centre frequency for the channel.

The downlink Doppler will be in the order of 11 KHz. maximum, and will require the receiving station to provide a.f.c. on his own receiver. Suitable circuits for this will be published in a later article.

This, then, summarises the f.m. system. With well-equipped stations, "press to talk" QSOs should be possible for most of the time that the satellite is "visible" between two ground stations. If all goes as planned, Amateurs throughout the world will have the unique opportunity to assess the suitability of all modes of communication by using both satellite transponders.

[An artist's impression of the type of satellite that OSCAR 6 will probably be is featured on the front cover of this issue.—Ed.]

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1970 John Moyle Memorial National Field Day Results

Certificate winners are indicated in bold type.

SIX-HOUR DIVISION

Section A:		
AX1AR/P2	432	points
VK2RJ/P	197	"
VK2ZCT/P	73	"
AX3ZA/P	492	"
VK3AIH/P	398	"
AX3UJ/P	321	"
AX3ASV/P	136	"
VK3FW/P	94	"
AX3AHG/P	75	"
AX4GT/P	358	"
VK4PJ/P	313	"
AX4SF/P	188	"
AX5QK/P	217	"

Section B:		
VK2YB/P	114	points
VK2JM/P	100	"

Section C:		
AX3HE/P	272	points
AX3EZ/P	160	"

Section D:		
AX3RZ/P	637	points
AX3BBC/P	452	"
AX5LP/P	186	"

Section E:		
AX1DH	275	points
VK4UG	90	"
AX9KY	109	"

Section F:		
L2390—S. Voron	450	points
L2949—K. Nad	90	"
L4—S. Dellit	410	"
L4018—C. Thorpe	130	"
L5015—W. Clayton	158	"
L7043—K. Everett	270	"
L7031—B. Mutton	255	"

24-HOUR DIVISION

Section A:		
AX3ZAZ/P2	154	points
AX3DY/P	1463	"
AX3BBR/P	714	"
VK3AOT/P	73	"
VK4ZDR/P	268	"
AX3ZE/P	568	"
VK5ZFE/P	118	"
VK5ZBT/P	128	"

Section B:		
No entry.		

Section C:		
No entry.		

Section D:		
AX1ACA/P	2947	points
AX2AAB/P	8091	"
VK3APC/P	6808	"
VK3AOT/P	4619	"
AX3ATL/P	3460	"
AX3AWL/P	2473	"
AX3XK/P	2233	"
AX3ER/P	721	"
AX4IO/P	1038	"
AX9XI/P	761	"

Section E:		
AX3KS	175	points
AX3XB	175	"
AX8KA	285	"

Section F:		
L3383—C. McLachlan	1625	points
L3308—A. Cox	740	"
L3312—M. Batt	535	"
L3—D. Harrison	270	"
L3042—E. Trebilcock	185	"
L4323—M. Joyce	510	"
L4104—K. Cunningham	315	"
L5113—L. Earle (Mrs.)	1518	"
L5098—T. Hannaford	1257	"

Check Logs:
AX3QV, AX9DR, and VK7RY

COMMENTS

The Field Day results this year showed a slight upward trend in the number of logs entered. However, the actual number of operators and assistants of multi-operator stations jumped to much higher figures than ever before. It would appear from checking the logs that the trend was towards greater group efforts from club stations.

From the logs, comments received indicated that the single operators would prefer the contest held on days that do not clash with the A.R.R.L. Contest, while the multi-operator stations are content to let the dates coincide.

VK5LP and VK5QZ are worthy F.D. operators. Conditions in the caravan at 1600 ft. in the Mt. Gawler area were such that temperatures reached 112° in the van at 10.30 a.m., and at noon the transistor heat sinks were too hot to touch, so rather than ruin the transistors, they closed down. However, they are undaunted, and will be out again next year. L2949 stated in his log that he had never heard a poorer contest, and what will the F.C.M. do for improvement?

Eric Trebilcock weighs in with the very pertinent comments "that it should be mandatory for S.W.I.s to log the serial numbers received—it's a farce as it is now."

Our Region Three W.I.A. Director condescended (or just "conned") to write out the logs for VK3AW/P this year, but had a problem with the 20 metre logs: "they" lost them!

For the operation of AX3APC/P, VK3AKJ writes "Two teams were entered by the Moorabbin Club for the 1970 N.F.D. One team operated under the call sign VK3XK/P and the other under the Club call sign of VK3AP/P. In addition at least six other Club members were Portable for all or part of the week-end."

"The Club station was situated at Mount Blackwood, some 50 miles north west of Melbourne in the Pentland Hills. The site had all the advantage of being some 2,000 ft. above sea level with a first class v.h.f. aspect of Melbourne and Geelong, and an excellent take-off for the short path to the States on h.f. However, the site was a comparatively small one since the 'plateau' on the hill top was surrounded by sharp drops on all sides and the useable part was not more than 70 yards square. There was, not unexpectedly, some mutual interference between equipment

"The comparatively small operating crew, some of whom were new to field day activity, had been in training for some weeks beforehand, especially in regard to the setting up of masts and antennas. This prior activity paid off, and probably for the first time, nothing was forgotten, everyone got there on time, all gear and tents, etc., went up on schedule and without even the slightest problem.

"The self-congratulation on this side of things just had to be short lived! It was!

"Around 0300K on the Sunday morning a near gale blew up and continued for over four hours. The 80 metre antenna literally blew away, the 15 metre quad was completely wrecked and the 20 metre beam lost one half of its reflector. No tents actually blew down, but only because of some very prompt rigging action by those affected.

"After a couple of hours 'make-do-and-mend', the site was operational again with makeshift antennas on 80, 15 and 10 metres and the 20 metre monster operating as a two element device.

"As always, a close watch was kept on the progress of other friendly rivals in the field to see how numbers compared. The conclusion was drawn at the end of the day that the result was going to be very open since at least three teams (including VK3APC?) appeared to be fairly close together in total number of contacts

"The general consensus of opinion at the end of the Contest was that next year our engineering has to improve and some better technique be found to wring numbers out of overseas 'clients'.

"Perhaps the Contest Committee would consider the possibility of relaxing the requirement of a serial number from other than VK stations, especially if our Contest again coincides with the A.R.R.L. Contest."

AX1ACA/P writes that the VK2 Field Day and the National Field Day clash caused some confusion. Operation via repeaters was also mentioned and also that the Rules should state whether or not repeater operations should be allowed for contest working

AX4GT suggests improving the Contest by awarding a certificate for top scorers in each section of all call areas.

Harold Burfoot, on behalf of his group, writes how they did enjoy the Contest, and on the high percentage of young people in their group. He throws out a challenge to all stations in next year's Contest. They had fourteen people involved, eight of whom were under 18 years of age.

Results this year have been published later than usual due to other magazine commitments. Also please note that the dates for next year's Contest are 13th and 14th February, 1971.

In conclusion, thanks to all who participated and submitted logs, and congratulations to the award winners

—Neil Penfold
Federal Contest Manager, for
Federal Contest Committee.

REMEMBRANCE DAY CONTEST, 1970

A perpetual trophy is awarded annually for competition between Divisions. It is inscribed with the names of those who made the supreme sacrifice, and so perpetuates their memory throughout Amateur Radio in Australia.

The name of the winning Division each year is also inscribed on the trophy and in addition, the winning Division will receive a suitably inscribed Certificate.

Objects

Amateurs in each Call Area, including Australian Mandated Territories and Australian Antarctica will endeavour to contact Amateurs in other Call Areas on all bands. Amateurs may endeavour to contact any other Amateurs on the authorised bands above 52 MHz. (i.e. intrastate contacts will be permitted in the v.h.f./u.h.f. bands for scoring purposes).

Contest Date

0800 hrs. GMT Saturday, 15th August, 1970, to 0759 hrs. GMT Sunday, 16th August, 1970.

All Amateur Stations are requested to observe 15 minutes' silence before the commencement of the contest on the Saturday afternoon. An appropriate broadcast will be relayed from all Divisional Stations during this period.

RULES

1. There shall be four sections to the Contest:—

- (a) Transmitting Phone.
- (b) Transmitting C.W.
- (c) Transmitting Open.
- (d) Receiving Open.

2. All Australian Amateurs may enter the Contest whether their stations are fixed, portable or mobile. Members and non-members will be eligible for awards.

3. All authorised Amateur bands may be used and cross-mode operation is permitted. Cross-band operation is not permitted.

4. Amateurs may operate on both Phone and C.W. during the Contest, i.e., Phone to Phone or C.W. to C.W. or Phone to C.W. However only one entry may be submitted for sections (a) to (c) in 1.

An open log will be one in which points are claimed for both phone and c.w. transmissions. Refer to Rule 11 concerning Log entries.

5. For Scoring, only one contact per station per band is allowed. However, a second scoring contact can be made on the same band using the alternate mode. Arranged schedules for contacts on the other bands are prohibited.

6. Multi-operator stations are not permitted. Although log keepers are permitted, only the licensed operator is allowed to make contact under his own call sign. Should two or more wish to operate any particular station, each

operating, then the word "log" followed by their own call sign, e.g., "CQ Remembrance Day from VK4BBB log VK4BAA."

C.W.: Substitute operators will call "CQ RD de" followed by the group call sign comprising the call of the station they are operating, an oblique stroke and their own call, e.g., "CQ RD de VK4BBB/VK4BAA."

Contestants receiving signals from a substitute operator will qualify for points by recording the call sign of the substitute operator only.

7. Entrants must operate within the terms of their licences.

8. Cyphers—Before points may be claimed for a contact, serial numbers must be exchanged and acknowledged. The serial number of five or six figures will be made up of the RS (telephony) or RST (c.w.) reports plus three figures, that will increase in value by one for each successive contact.

If any contestant reaches 999 he will start again with 001.

9. Entries must be set out as shown in the example, using ONLY ONE SIDE of the paper and wherever possible standard W.I.A. Log Sheets should be used. Entries must be clearly marked "Remembrance Day Contest 1970" and must be postmarked not later than 6th September, 1970. Address them to "Federal Contest Manager, W.I.A., G.P.O. Box N1002, Perth, 6001, West. Aust." Late entries will be disqualified.

10. Scoring will be based on the table shown.

SCORING TABLE

		To									
		VK0	VK1	VK2	VK3	VK4	VK5	VK6	VK7	VK8	VK9
From	VK0	-	6	6	6	6	6	6	6	6	6
	VK1	6	-	1	1	2	3	5	4	6	5
	VK2	6	3	-	1	2	3	5	4	6	5
	VK3	6	4	1	-	2	1	4	3	6	5
	VK4	6	3	1	2	-	3	6	5	4	3
	VK5	6	5	2	1	3	-	4	3	6	6
	VK6	6	6	2	1	4	2	-	3	6	6
	VK7	6	5	1	1	3	2	5	-	6	6
	VK8	6	5	1	1	2	3	6	4	-	3
	VK9	6	5	1	2	3	4	6	5	1	-

Note.—Read table from left to right for points for the various call areas.

In addition, all intrastate contacts on 52 MHz. and above are worth 1 point each per band.

Portable Operation: Log scores of operators working outside their own Call Area will be credited to that Call



Remembrance Day Contest Trophy

will be considered a contestant and must submit a separate log under his own call sign. Such contestants shall be referred to as "substitute operators" for the purposes of these Rules and their operating procedure must be as follows:—

Phone: Substitute operators will call "CQ RD" or "CQ Remembrance Day" followed by call of the station they are

EXAMPLE OF TRANSMITTING LOG

Date/Time G.M.T.	Band	Emission and Power	Call Sign Worked	RST No. Sent	RST No. Received	Points Claim.
Aug. 70						
15 0810	7 Mc.	A3 (a)	VKPS	58003	—	1
15 0812			VKRU	58007	—	1
15 1035	20 "	A3 "	VKZAZ	58010	—	2
15 1040			VKZAL	58020	—	2

Note.—Standard W.I.A. Log Sheets may be used to follow above form.

EXAMPLE OF RECEIVING LOG (VICTORIAN S.W.L.)

Date/Time G.M.T.	Band	Emission	Call Sign Heard	RST No. Sent	RST No. Received	Station Called	Points Claim.
Aug. 70							
15 0810	7 Mc.	A3 (a)	VKPS	58003	—	VKRU	1
15 0812			VKRU	58007	—	VKZAZ	2
15 1035	20 "	A3 "	VKZAZ	58010	—	VKZQR	2
15 1040			VKZAL	58020	—	VKZQV	2

Note.—Standard W.I.A. Log Sheets may be used to follow the above form

Area in which operation takes place, e.g. VK5ZP/2. His score counts towards N.S.W. total points score.

11. All logs shall be set as in the example shown and in addition will carry a **front sheet** showing the following information:—

Name Section
Address Call Sign
Claimed Score
No. of Contacts

Declaration: I hereby certify that I have operated in accordance with the Rules and spirit of the Contest.

Signed

Date

All contacts made during the Contest must be shown in the log submitted (see Rule 4). If an invalid contact is made it must be shown but no score claimed.

Entrants in the Open Sections must show c.w. and phone contacts in numerical sequence.

12. The Federal Contest Manager has the right to disqualify any entrant who, during the Contest, has not observed the regulations or who has consistently departed from the accepted code of operating ethics. The Federal Contest Manager also has the right to disallow any illegible, incomplete or incorrectly set-out logs.

13. The ruling of the Federal Contest Manager of the W.I.A. is final and no disputes will be discussed.

Awards

Certificates will be awarded to the top scoring stations in Sections (a) to (c) of Rule 1 above, in each Call Area, and will include top scorer in each Section of each Call Area operating exclusively on 52 MHz. and above. VK1, VK8, VK9 and VK0 will count as separate areas for awards. There will be no outright winner for Australia. Further Certificates may be awarded at the discretion of the Federal Contest Manager.

The Division to which the Trophy will be awarded shall be determined in the following way.

To the average of the top six logs shall be added a bonus arrived at by adding to this average the ratio of logs entered to the number of State Licensees (including Limited Licensees), multiplied by the total points from all entries in Sections (a), (b) and (c) of Rule 1.

Average of top six logs +

Logs Entered	Total Pts. from
State Licensees ×	all Entrants in
includ. Z Calls	Section (a) (b) (c)

VK1 scores will be included with VK2, VK8 with VK5, and VK0 with VK7. Also, VK9 logs and score will be added to the Division which is geographically the closest.

Acceptable logs for all Sections shall show at least five valid contacts.

The trophy shall be forwarded to the winning Division in its container and will be held by that Division for the specified period.

RECEIVING SECTION

(Section D)

1. This section is open to all Short Wave Listeners in Australia, but no active transmitting station may enter.

2. Contest times and loggings of stations on each band are as for transmitting.

3. All logs shall be set out as shown in the example. The scoring table to be used is the same as that used for transmitting entrants and points must be claimed on the basis of the State in which the receiving station is located. A sample is given to clarify the position.

It is not sufficient to log a station calling CQ—the number he passes in a contact must be logged.

It is not permissible to log a station in the same call area as the receiving station on the m.f. and h.f. bands 1-8

30 MHz., but on bands 52 MHz. and above such stations may be logged, once only per band, for one point. See example given.

4. A station heard may be logged once on phone and once on c.w. for each band.

5. Club receiving stations may enter for the Receiving Section of the Contest, but will not be eligible for the single operator award. However, if sufficient entries are received a special award may be given to the top receiving station in Australia. All operators must sign the Declaration.

Awards

Certificates will be awarded to the highest scorers in each call area. Further Certificates may be awarded at the discretion of the Federal Contest Manager.

THE W.I.A. TIE

At the Federal Conference in Adelaide last Easter it was decided to obtain a tie which could be worn by members of the Institute. A design was proposed at the meeting and after consultation with the tie makers it is now ready for production. The illustration shows the general conception. Two ties will be available, one in navy blue and



the other in deep red or maroon, and the material will be washable terrylene. Each will have a single small W.I.A. badge with the map in white and the detail in red.

Colour photographs and colour slides showing the samples in full colour are being circulated to all centres and orders are awaited. We feel sure that the tie will be well received because

it is a very handsome tie and will do justice to almost any suit.

Sales will be on the basis of cash with order, and ties will only be ordered after the money has been received at W.I.A. headquarters. The price to members will be about \$2.50 and the delivery time will be about five months. Division Secretaries are requested to get their orders in quickly so that the first batch can be ordered without delay.

FEDERAL PRESIDENT OVERSEAS

The Federal President of the W.I.A., Mr. Michael Owen, VK8KI, left on 18th June for a world tour which is expected to last six weeks. Whilst overseas he will be visiting Amateur Societies for discussion with their officials and arrangements have been made for him to meet officers in Philippines, Hong Kong, Japan, India and Thailand.

His tour will include U.S.A., England and Europe. It is hoped that talks with A.R.R.I. and I.A.R.U. officials in these countries will provide information on I.T.U./I.A.R.U. affairs that will assist the Institute and Region 3 organisation in their Space Conference proposals.

Although part of Michael's trip will be concerned with business, the primary aim in many ways is essentially Amateur/I.T.U. orientated. Federal Council have agreed that part of the expense should be borne from I.T.U. funds and the Region 3 organisation has also made a contribution of \$300 with additional assistance from "A.R."

Federal Council and Executive are looking forward to frequent taped reports on his encounters, which will be published in "A.R."

BECKETT FESTIVAL STATION, GB2CF

7, Old Ford,
Cheshfield,
Whitstable, Kent,
England

Secretary, W.I.A.,

Dear Sir,

We should be very grateful if it could be brought to the attention of Radio Amateurs in Australia of the Beckett Festival Station, GB2CF, active from Canterbury, England, from 19th to 20th July inclusive.

This station will form part of the Beckett Festival, and QSOs which will be QSLed with a suitable card, will be most welcome. QSOs with stations in towns in Australia called Canterbury or any of the following local towns and villages which surround our city would be most welcome.

Ash, Ayratham, Bechesbourne, Bridge, Chillingham, Chartham, Faversham, Eltham, Herne Bay, Herne, Isatham, Kinton, Littlebourne, Patricbourne, Sturry, Selling, Stelling, Wye, Wingham, and Wickhambrux.

Yours sincerely,

G. Smith, GB2CUC
(Acting in co-operation with
GB2LCK, GB2XDV, GB2XWQ)

NEW CALL SIGNS

FEBRUARY 1970

VK1EB—F. F. Bacon, 7 Munsey St., Ainsley, 2602
VK1ZV—G. A. Cohen, 39 Quondam St., O'Connor, 2601
VK1EM—School of Applied Elect., Sydney Technical College, Harris St., Uthman, 2007
VK1GR—A. B. Mason, 18 Queens Rd., Asquith, 2078
VK1IO—R. E. Durrant, 12 Harper St., North Kippin, 2121
VK1OA—W. J. Lark, 9 Cosimo St., Toongabbie, 2140
VK1AJZ—C. E. Haycock, 17 Ivanhoe St., Marwickville, 2204
VK1ATW—T. E. Whitfield, 1/41 Ross St., Onley, 2223
VK1BJJ—J. B. Stacy, Station: Panorama Rd., Calala, 2340; Postal: R.M.B. 822C, Panorama Rd., Calala, 2340
VK1BLA—W. L. Laird, 63 Kentucky St., Armidale, 2350
VK1BSL—K. M. Cunningham, 35 Marshall St., New Lambton Heights, 2305
VK1BWJ—W. Robertson, 80 Albany St., Coffin Harbour, 2450
VK12IT—S. R. Gregory, 5/137 Cowper St., 2000
VK12PZ—W. Frost, 98 Young St., Cremorne, 2000
VK12YR—D. L. Dwyer, 3/26 Brittain Cres., Hillsdale, 2038
VK13AX—F. W. Heaps, 383 Bridge Rd., Richmond, 3121
VK13AU—R. C. Gual, Station: "Reta Park," Ringwood, 3164; South Warrandyte, Postal: 88 Montego Key, Navato, California, U.S.A. 94047
VK13BS—W. T. R. Ward, 220 Cardigan St., Carlton, 3003
VK13BT—D. O. Taylor, 3 Elia Crt., Eltham, 3085
VK13BU—P. B. Parry, 12 Milverton St., Moonee Ponds, 3039
VK13BV—J. T. Cunningham, 11 Catherine Pde., Frankston, 3162
VK13CF—C. Dicknell, 13 Roland Ave., Strathmore, 3041

VK13CO—G. J. Cohen, 10 Lemon Gr., Nunawading, 3131
VK13DA—D. V. Hambleton, 28 Jacqueline Rd., Mt. Waverley, 3149
VK13DK—K. H. King, 15 Stonehaven Cres., Moorabbin, 3168
VK13YAC—S. J. Whitehead, 285 Gellagheri Rd., Glen Waverley, 3150
VK13YT—H. Y. O'Hanlon, 10 Lyons St., Glen-humly, 3163
VK13YZ—C. L. Lane, Funnell St. South, Balaarat, 3230
VK13ZE—W. D. Powis, 17 Balfour Rd., Mt. Waverley, 3148
VK14YS—R. A. Sedunary, Riverside Caravan Park, North Rockhampton, 4701
VK14ZKV—R. H. Kyle, 17 Alden Ave., Southport, 4213
VK15LY—J. R. Godson, 4 Fairlie St., Ottaway, 5013
VK15SY—D. M. Smotherer, Travelsodge, Motel, South Tee, Adelaide, 5000
VK15ZLL—L. G. Douglas, 123 Flinders Tee, Port Augusta, 5705
VK15ZA—B. J. Lemay, 14 Gerlich Rd., Elmsbeth Park, 5113
VK15BK—P. Anderson, 16 Stone St., Maylands, 6051
VK15DS—A. W. Storm, 289 The Boulevard, City Beach, 6015
VK15KR—K. E. Reeves, 14 Pontiac Ave., Cloverdale, 6105
VK15LG—R. K. Lyon, 450 Riverton Dr., North Perth, 6155
VK15WB—A. F. Jacobson, apt. 3, Lot 5, Scott St., South Perth, 6155
VK15CID—L. W. Roobin, Station: Portside, Postal: 712 Glenhilly Rd., South Caulfield, Vic., 3162
VK15AG—G. E. Watts, Station O.T.C.I.A.I., Rem. S. Browns Range, Carnarvon, 6701; Postal: P.O. Box 96, Carnarvon, 6701
VK15TH—F. Foxon, 8 Elms Rd., Sandy Bay, 7005
VK15CE—R. J. Sieber, 28 Lindsay Ave., Alice Springs, 5750
VK15AC—T. Ivins, Station: Lot 1, Section 185, Jibarra Dr. Boroke, P. Postal: C/o. Posts and Telegraphs Training College, Racecourse Rd., Boroke, P.
VK15DZ—M. J. Groff, Station: Marty's Memorial School, Popondetta, P. Postal: P.O. Box 36, Popondetta, P.

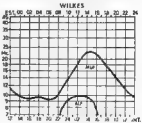
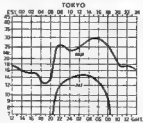
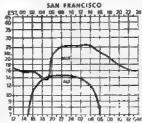
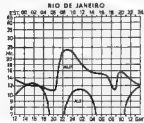
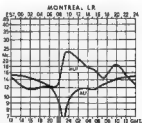
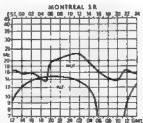
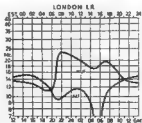
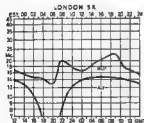
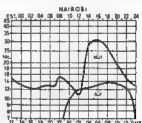
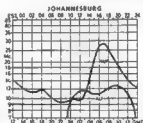
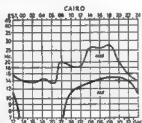
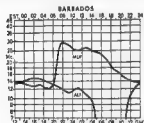
VK15GA—N. Spalding, Station: Section 8, Albotment 1, Kaviang, N.G., Postal: C/o. Posts and Telegraphs, Kaviang, N.G.
VK15HS—Station: Tuff Bryans Auto Port, Malaguna Rd., Rabaul, N.G., Postal: C/o. Airport Charter, P.O. Box 461, Rabaul, N.G.
VK15NS—R. S. Sleeth, Station: Norfolk Island, 2899; Postal: Box 223, Norfolk Island, 2899
VK15VT—V. T. Fresh, Rev. J. Catholic Mission, Lemakol, Kaviang, N.G.
VK15WF—W. Frost, Station: Port Moresby, P. Postal: P.O. Box 3185, Port Moresby, P.

CANCELLATIONS

VK17IO—R. K. Westbrook Now VK1KO
VK17OO—J. A. Gardner Transferred to Qld.
VK1ZAN—J. D. Cuffe Not renewed
VK12IS—M. E. Dason Transferred to W.A.
VK12OA—School of Applied Electricity Now VK12EM
VK12SO—W. P. Nobles Not renewed
VK12LK—W. J. Lark Now VK13LA
VK12EG—W. L. Laird Now VK13LA
VK12PZ—J. E. Andersen Transferred to Tas.
VK12HR—G. E. Watts Now VK15AG
VK12KC—K. M. Cunningham Now VK1BSL
VK12PO—C. L. Scally Transferred to T.F.N.G.
VK13FF—D. E. Spraw Not renewed
VK13AG—E. F. O'Brien Deceased
VK13IU—D. J. Tanner Transferred to S.A.
VK13AK—S. J. Whitehead Now VK15YAC
VK13KH—J. G. Cohen Now VK13CO
VK13MS—J. M. Bywaters Not renewed
VK13PP—P. M. Cohn Transferred to N.S.W.
VK13UO—W. G. Reynor Transferred to N.S.W.
VK14VJ—W. Jeffs Deceased
VK15DB—S. R. Brooks Not renewed
VK15CE—R. J. Sieber Now VK15CE
VK15AZ—B. A. Cook Transferred to Vic.
VK15CH—C. Hulse Transferred to S.A.
VK15DT—D. Trickett Transferred to Vic.
VK15VH—L. W. Roobin Now VK15CID
VK15AJ—G. Drage Not renewed
VK15BG—H. Baker Deceased
VK15DR—O. Lukin Not renewed
VK15LM—L. K. McPherson Transferred to N.S.W.
VK15RO—R. S. Gurr Not renewed
VK15AW—A. J. Watson Not renewed
VK15GA—N. Spalding, Now VK15GA.

PREDICTION CHARTS FOR JULY 1970

(Prediction Charts by courtesy of Ionospheric Prediction Service)



Sub-Editor: ERIC JAMIESON, VK3P
 Forrester, South Australia, 5233.
 Closing date for copy 30th of month.

AMATEUR BAND BEACONS

VK4 144.380 VK4VW, 107m. W. of Brisbane.
 VK3 53.890 VK3VW, Mount Lofy
 144.800 VK3VW, Mount Lofy
 VK8 52.000 VK8VW, Tuart Hill.
 52.900 VK8VW, Carnarvon
 VK1 144.380 VK1VW, Tuart Hill
 423.000 VK8VW, (arr by arrangement)
 VK3 144.800 VK3VW, Devonport
 ZL1 145.000 ZL1VW, Christchurch.
 JA 51.965 JA1VW, Japan.
 W 50.081 W8BKA, U.S.A.

A couple of items on the subject of beacons are noted in the May issue of the Western Australian V.H.F. Group News Bulletin. Firstly that at the Group's April meeting it was decided to tell the Mount Barker Beacon to the Southern Electronics Group—in the absence of other information we could only assume that the is a group of interested Amateurs in the Albany or near area, and who will keep the beacon ticking. The second item is that the Perth Tuart Hill Beacon was off the air from 20th April, with a proposal to re-instate them at the QTH of Tony VK8ZK. I hope the VK8s will keep me informed of any moves of the beacons so the list may be kept current. They have been listed complete this month.

Eric mentions continues to provide a lot of interest the notices are of this continent, and whilst some of the following news is a bit odd, it is still interesting to read. I am indebted to the VK3KXK in Darwin for the following: During April VK3VW worked DUMM in the Philippines on 62.120 MHz. Good work. Brian Doug said he missed this one as he was watching the wrestling on Indonesian TV!! On 22nd March, JAZAYM worked V888F (Hong Kong) on about 50.100, so that's an area we haven't thought much about before. Stan W6ABN reported in April the first trans-equatorial 80 MHz DX to South America for the season. Apparently there are many keen 8 metre operators up and down the West Coast of U.S.A. really keen to get into South America. ZK1AA is a regular to K8s, and the same station was very happy to work K8AQ recently! I would be too! Doug reports a number of stations being heard on backscatter. Tony VK8ZDZ being one, quite a considerable distance for such propagation. Thanks Doug for your interest, and I pass on your hint: "Watch 8 metres each evening from run-down to 1300z, 12 MHz and above for the JAs".

While still on 8 metre DX, Bob VK2ASZ provides an interesting run down of VK3 activity during the equinoctial period. He reports that John VK8T1 operates 5202Z A3, from Madras. VK8QA is another on 8 metres, while VK8ZKEN and VK8ZDZ 5355Z make the VK8 even a more favoured area for the coming DX season. Going back to the JA opening, on 25th April, reported in June issue, Bob says the first indications of something to happen in the Russian tv which appeared on 42.751 MHz, about 1200 EST, followed by ZL1 tv. He then worked Earl VK8VL, and noticed the beam direction had no effect. At 1330 JA1VW appeared, then VK4s at 80 plus with JAs in background. Between 1400 and 1515 Bob worked 14 JAs from all districts, and heard JAs working VK1, 2, 3, 4 and 7. ZL1 tv, Russian TV and JA1VW remained a constant S8 throughout. About this skip appeared the VK8ZDZ and he could hear the JAs concentrating on that State. Bob reported the skip appeared to move from JAL in Eastern Japan slowly to VK8 in the West with each area becoming in turn, and remarked it was most unusual to hear Ks and F3 at the same time. On checking the log, Bob could see a build up in the pattern of things. ZL1 tv on 81.750 was heard on 10 different occasions at good strength during March and April, while during the same period Russian TV on 42.750 was heard 12 times, and on no less than 4 occasions worked JAs, including 20 of them in an opening on 15th April. Thank you Bob, that has brought everyone up to date on your area.

Two metres seems to have been relatively quiet if the absence of news from most areas is any guide. Do note that Tony VK8ZDZ had a 5 x 9 contact with W1F VK7VW at 2300 EST on 23rd May, a good effort. Seemed to be too quick for everyone else to be in their shoes though.

Did hear a whisper on the air that some long distance workings had taken place in VK4 during May on 432 and/or 1260 MHz. My efforts to get anything further on this have met with no response.

MEET THE OTHER MAN

Bob Lear, VK2ASZ, of 179 Rusden Road, Blackland, first commenced Amateur operations in 1955, and was since left his mark on v.h.f. activity. He works as a v.h.f. 2-way radio service technician, but has branched out into other fields as well. He has held a Private Pilot's Licence for 15 years, and occasionally goes 148 MHz aeromobile! Last year he completed 4 years' training for Flight Navigator seems to be a terror for punishment! Married, with two children, Bob has certainly put a lot of effort into his Amateur operating, both 8 h.f. and h.f.

He runs 100 watts on 8 metres using parallel 4140z to a 6/8 antenna 35 ft. high, 425BZ modulator, 625B cascade converter His 144 MHz gear also runs 100 watts of a.m. to a Q202M/40, 10 over 10 slot antenna 50 ft. high, 220CC cascade converter, modulator push-pull 4DQz. The tunable 10 for these two bands is an SX100 Hallcrafters, 30 watts of a.m. provides a nice signal on 432, using a QQ202/20 to an 11 element yagi 50 ft. high. Converter uses ZC69 crystal stages of grounded grid to a 1N21 crystal mixer, fed into the 6 metre converter. Also operates 80 through 10 metres with a Drake TK3 w.b.s. machine.

Areas worked on 8 metres include VK1 to 9 inclusive, ZL1 to 4 inc., JAL to 9, JAs, Willis 12 (VK8), and Papua (VK3). On 144 MHz, VK1 and 2, ZL1, 3 and 9, and VK1 and 2 on 432 MHz. He has also operated on 10,000 MHz, for a short while. He originally held the 144 MHz Australian record for three years from his 31/12/81 for his contact with ZL3AQ, he has received for 50 MHz, W.A.S. V.H.F.C.C. 30, V.S.F.C.C. 144, A.I.D. several Ross Hull Contest Certificates, and recently claimed D.X.C.C. and W.A.C. for h.f. contacts.

He is a member of the W.I.A. and during 1968 and 69 was Secretary and V.h.f. Scribe for the VK3 V.h.f. Group. His plans for the future include building equipment for 1300 MHz, more on 10,000 MHz, continuing with television experiments, and will soon be trans-

mitting pictures on 432. He will be trying very hard to work ZL1 on 144 MHz in 1974, 75, and also New Zealand on 432 at the same period. His location is Blackland, 45 miles west of Sydney, in the lower Blue Mountains, 650 feet above sea level.

Bob also mentions that he has arranged facilities so he can take out his whole station portable, and has often done so for v.h.f. field days and national field day. During the past several years he has tried various mountain tops over much of N.S.W. from Mt. Ebor 300 miles to the north, to Snowy Mountains in the south. These latter he has given away as they are too cold. He will run 100 watts portable in big beams, but the overall result for long distance working have been disappointing. This invariably seems to be the case with all of us on mountain tops—B.L.P. Bob does operate on net frequencies, but would like to see many operators on such frequencies try the DX to be had on other portions of the band. He throws in a final comment, that although he does a lot of work with solid state equipment, he is far from convinced that valves have been replaced by transistors for serious v.h.f. work!

STOP PRESS

What is probably the first ever 5 metre contact between VK and V3 was made on 2nd June by VK8KK and V36DA. More details will be included in the v.h.f. notes next month.

VK8s are reminded of their Intra-State Contest scheduled for Sunday, 28th July. The VK3 Contest Committee has studied last year's results closely, and amended the rules where desirable. Full details have been published in the "South Australian Journal", but brief, you are reminded that one of the aims of the contest is to bring the v.h.f. and h.f. operator closer together by giving incentives for cross band working between the two sets of bands.

None of my usual scribes have written this month so news is a bit scarce. However, the Editor will appreciate this after the big two-page spread last month! We will close with the thought for the month: "Men may be convinced, but they cannot be pleased, again!" until next month, 32, Eric VK8LP The Voice in the Hills.



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Bus-Editor DON GRANTLEY
P.O. Box 222, Panth, N.H.W., 2780
(At times in GMT)

Again we have a gradual decline in conditions, although there have been some fantastic reports of 30 meters. Although the higher frequencies have slackened off, there is a gradual upswing on 40, if you can battle the interference, also on 40 and 32. At the time of writing the latest confirmation was 18 for January.

There have been some good operations over the May period, most important could well be the San Marino efforts from DJ9MJ, DK3RZ and DL3RL. QSLs for these stations go to their home addresses. Other good ones were the 707T/FC operation by GB8ID, QSLs to W3CTN, also Zambian activity by 9HR/LA, whose manager is VJ2QDX, Box 111, Postal Station "Q", Toronto 7, Ontario.

GB3CF is the call of the station used for the Festival at Canterbury during the period 19K to 1915 July inclusive. I understand a special QSL is available. Details elsewhere this issue Ed.

GB3FON will be the call of the station covering the Festival of Nottingham which runs from 11th to 26th July. Frequencies for the latter are 1920, 2760, 7060, 14260, 21860 and 28060. An attractive Robin Hood Emblem QSL is to be sent to all stations confirming contact with the Festival station.

I have mentioned the activity of King Hussein JY1 quite regularly over the past three months, however it will be admitted that this operation is worthy of mention in passing. The King Hussein Club, the bodies which have played his activities and I reported last month that well known ace Wayne W1MBD/I was the operator, the latter a well known ace to clear the air a little. It has since been reported that WASHUP and OM W3GR have made a three-day visit to the King Hussein net. WASHUP said a WA was due to go and assist from 18th May.

Recently reported from Kura is by KM4DD/K4R4 could be the call of the QSL information which is Box 190, P.O. San Francisco, California, 94614. Evidently the wrong zip code was issued in the first place. A well known ace Alan Thor Heyerdal has set out on a cross Atlantic voyage, this time in "RA 11". He is equipped with radio gear, and when power is available he will be on using the call RA 11B. This has been heard in the U.K. working WA2TO and LISA, the latter being the official call of LANSKO for traffic purposes. The frequency in use was 14314 s.b., and the time of operation 1510.

TCO is a special, prefix being used by stations in Istanbul over the last week-end in May to commemorate the completion of that city. All QSOs will be confirmed by a special QSL, and there is an award available for working the Istanbul stations during 1969 and 1970 May, and 1969, 31st May. All bands and modes and a station can be counted again if worked on another band. The call is TCOA, Box 69, Istanbul, Turkey, by 1901 July. The stations eligible are TCOAE, AV, DE, EA, NY, IB, XT, MT, NC, NF, OR, QR, VO and ZL.

W4BFD should be active now. He was expected to leave New York on 28th May, arriving in Kenya the next day. The F.R.C.A., Box 69, Nairobi, Kenya, has endorsed for operation on most if not all French possessions, so he could turn up anywhere at any time. His frequencies are 1900-1910, 2760-2770, 7060-7070, 14160-14170, 21860-21870, 28460-28470. All QSLs now go to W4BFD.

John V35JK was due back home to G-land on 26th May, and asks that all requests for QSLs from his V35 operation go to home QSL G3KJF.

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March 1976—

Solid State Circuits for S.S.B., CLABD. Part 2 of a 3 W. Herbert of the Central Institute of Technology, Petone.
Swedish Unit for the Heathkit Band Transceiver, ZLAVP. A description of a simple, solid state squelch unit.
TV Tuners and V.M.F. Converters, ZLIBAU. A modified tv tuner makes a handy v.h.f. converter which covers a number of bands. The writer has seen designs using older style tuners, which covered frequencies right down to about 80 metres.

No. 69—

After Glow. Discusses various types of phosphor which are available and the advantages and disadvantages of each for Amateur TV.

ATV Demonstration at Harwell—

ESTV. A note on the equipment used by Prof. Franco Panti, ICLF, of Bologna, Italy. Main object is to solicit contacts with others similarly equipped.

Videoen Blanking Generator. Describes a small unit for flyback blanking.

"CQ"

March 1976—

Safe and Sound Tower Installation, Part 1, WENZ.

A Homebrew All Solid State Communications Receiver, WENZ. Tunable 1.6 to 3.05-3.125 MHz. working into mechanical filters on 486 KHz. Front-end converters are crystal controlled.

"CQ" Reviews the Heathkit HQ-100 V.F.O., WLAZY. Uses a 6CH6 and OES regulator.

A Pre-Amplifier for Tube-Type Transceivers, WEEZY. Take your choice of 6BX7 and 12BE6 to add selectivity and gain to transceivers in need.

The Invisible Beam, WOGHX. A fantasy in the construction of a beam antenna by a very smart Amateur with plenty of "dough". Automation gone wild!

Modern Remote Tuning, WEEZY. Motor driven diodes can be replaced by precision diodes and lamp-photocell modules. Various techniques are discussed and sample circuits are included from several transceiver units.

All About Microphones, WEEZY. A useful article which will inform the novice and refresh the memories of DXers.

A Handy-Dandy Variable A.C. Supply, K3BTU. A boxed Variac with metering.

An A.W. High Powered Amplifier, WACJL. Operating on 40 and 40 and using a pair of 1-100As in the "Doherty" circuit.

A Solid State V.L.F. Converter, WEEZY. WHITT. One transistor and one IC.

April 1976—

An All Band 4CX1008A Super Cathode Driven Amplifier, TIGVL. There is always something new to work on.

A Simple D.C. to D.C. Converter, KAPZW. The tv flyback transformer core finds its way into Amateur Radio to supply voltages for a transceiver. Will the copiers please tell me why he broke one leg?

Notes on Transistorised Transceiver Considerations, VE2BIR. Calls upon some commercial experience to make some suggestions for use in Amateur Radio.

A G. E.T. Central Layout, WOPHY. Short and sweet switching system.

A Cheap and Clean Scope Card, Jim Ashe. Taking mahomet to the mountain!

Tags . . . A Submerged Antenna Propagation System for Enhancing DX, ex YMAKR Grant v.h.f. DX. Underwater.

"HAM RADIO"

Broadband Double-Balanced Modulator, by WA8NCT. Practical construction details of a hot-carrier diode mixer that covers the range 200 KHz. to 100 MHz.

Compact Dual Band Antennas, WESAL. Simple but effective antenna systems for city-lot dimensions or smaller.

Tunable Peak-Notch Audio Filter, John H. Schultz. Solid state circuits featuring the twin-T network—useful in test equipment or for improving receiver selectivity.

Further Automation for Typewriter Type Electronic Keys, W6RPO. A buffer storage unit is described which increases the versatility of the "Pro-Key" marketed by the Micro-Z Co. **Homebrew Five-Band Linear Amplifier, by WTV.** Constructively conservatively designed, time proven 6AL5A per, of these tubes operating with B plus of 1500 volts is about the right power input to meet the VK licensing requirements.

A New Approach to Equipment Rack Construction, KICCL. Here's a low cost rack that can be easily built to accept any panel width. It believe the material used in this job is obtainable in Australia under the name of "Uni-Strut".

Solid State Radio Direction Finder, WJTT. D.F. principles are detailed and various methods are described (Will this bring the tx hunt back?).

A Power Amplifier for 100 MHz., WCCCY. Dual planar triodes in a half-wave resonant cavity provide 100 watts output with 10 dB power gain.

A Low Power Solid State Transmitter for Two Meters, W. G. Enlick. The will to improve and salvaged tv parts, resulted in this little bomb.

Economical Beams for Ten Meters, WITFF. Improving the "Wonderbeam" antenna for effective DX work.

A Stable Small-Signal Source for 144 and 432 MHz., KAJC. This simple circuit features variable frequency coverage and uses a reference signal for v.h.f. converter adjustments.

Regenerative Detectors and a Wideband Amplifier, WTSYB. Easy projects to acquaint you with transceiver circuits with hints on determining the correct component values and some good advice on power supply design.

April 1976—

It is perhaps unusual to begin a review by discussing an advertisement, but on page 9 of this issue Swan announces a new 10 crystal filter with a 6 dB bandwidth of 27 KHz., 60 dB bandwidth of 3.475 KHz., 120 dB bandwidth of 4.9 KHz. and an ultimate rejection exceeding 140 dB. Price is quoted as \$85 (in U.S.A.) to Swan users only. Some filter!

Operational Power Supply WAAKIL. Regulated d.c. supply, low-frequency amplifier, current amplifier, with bipolar output—these are just a few uses for this unit.

A Simple Speech Processor for S.S.B., K3PHT. Using a FET input stage and four bipolar transistors, this speech processor is stated to increase the effective speech level by about 10 dB whilst maintaining distortion at a low level.

An Electronic Thermometer, VK2ZNV. A simple but effective instrument that can be built in just a few hours.

Catalina Wireless 1005, WESLZ. Another glimpse into the early days of Radio by an old timer who has been around for a long time.

Variable Bandpass Audio Filter, G. B. Jordan. One solution to the receiver selectivity problem is this RC feedback system featuring variable bandwidth from 50 Hz. to 10 KHz.

V.F. Power Amplifier, for 486 MHz., KAJC. 100 watts input on c.w. and 85 watts on a.m. to 3004. Featuring resonant line tank circuit and class C output.

Improving Overload Response in the Collins 75A-4, WEZO. Simple modifications provide 13 dB higher signal handling capability in this fine receiver.

Direct Reading Capacitance Meter, ZL3AUE. An easily built instrument with many uses around the workshop.

Twenty Four Hour Digital Clock, KAJLS. With nice readout.

A Low Power Dummy Load and P.E. Wattmeter, W3OLU. An accurate and reliable test instrument which is low in cost. Uses an old thermocouple r.f. ammeter calibrated in watts into four decibels.

How to Use a Sweep Generator, Larry Allen. Takes the newcomer to the repair bench and shows him how.

An All Band Ten dB Power Attenuator, by KICCL. This device can be used as a transmitter interstage buffer or for isolation when making antenna S.W.R. adjustments.

"QST"

March 1976—

An Engineer's Ham Band Receiver, DL5WD. An all solid state design for the experienced constructor. The h.f. local oscillator uses a frequency stabilized technique. Single conversion design using KVG 9 MHz. filters.

High Versus Low Antennas, KEYNE. Compares the performance of identical antennas mounted side by side at different heights. Experimental evidence is given to support the case for increased antenna height for better results.

A Simple Signal Feeder for Crank-up Towers, KJHJ. Preventing wind pawl slip. **Transmitting QRP by Technician, WJCEK.** Transmitter SW from 12, receive a few mA. peak current 800 mA. All solid state. **The K4003 10 MHz. Kilowatt Amplifier, K4003.** Efficiency at the top end of the v.h.f. range.

A Two Element 15 Metre Quad for the Novice, WBBJC. Sprinklers are combination of aluminum and plastic water pipe.

A Ca-anal Switch with all Unused Contacts Shunted to Ground, WILCP.

Let's Talk Transistors, Part 5 Transistor Circuits, Robert E. Stoffia.

A Trap Filter Duplexer for 3 Metre Repeaters, WIKKE. Keeping transmitter power out of the receiver.

April 1976—

The Modulator ST-3 R.T.T.V. Demodulator, W4PCT. Two versions are actually described. The ST-3 for 850 Hz shift and the ST-4 for 170 Hz. Small and solid state.

A Receiver with a Wideband Pre-Amplifier, by WILCP. An FET pre-amplifier for those whose receivers have insufficient front-end selectivity and gain.

Improved 15 Metre Portable Performance for a Mobile Station, W8RTT. attaches 80 ft. of wire to his mobile whip below the loading coil and in limited space without getting off the ground. Which is the harder, digging a 35 ft. well, or climbing a tower?

A Skinnier Linear, WICER. Describes a grounded grid linear using an Amperex 6L6 40-watt plate dissipation colour tv. line scan pentode. 'Phillips cannot supply them in Australia.

Clamping Diodes for C.W. Break-in, WBSZ. A dozen diodes and the doovers done.

Receiver Indicators for the Linear Amplifier, Sensitivity and Transmitter Output from the Heath HW-17A, WINDQ. Thanks for the review, Ed.

Using the Tassas Mason VT656 Six Metre Transverter with the 8/Lines, KJHJ. Mr Collins may not like it, but Fred will not object.

Using Indicators for the Linear Amplifier, WIKLIK. There appears to be more to this subject than a simple "dip and load".

Radiated Pattern of a Dipole over Perfect Ground, K4GEX. For the academic.

"RADIO COMMUNICATION"

March 1976—

Reps and Rigging for Amateurs, QJUMQ. A review of a book (of the type) is a Board of Trade certificate yachtman's Ocean and he knows his ropes. Every Amateur needs a basic understanding of this subject so that his vessel will be a safe one.

Receiving Amateur T.V. Transmissions, by G4UUTV and G3YFV. How to get started in receiving short article by ZB60, titled "operation is discussed". V.H.T./V.H.F.

A Facility for the Top Band to Ten S.B. Transmitters, G3HVA.

Using a G3EVT Test Falsar, G3SEK/Z3STC. Designed to be used for the adjustment of linear amplifiers or for chasing T.V.

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of valves. Valve and solid state circuits are covered.

TE2002 Conversion for Two Metres, GABUS. A useful transmitter/receiver combination which can easily be converted to two metre operation and makes an excellent "stand-by" unit.

Calculators Simplified, GSPEP. Could be of considerable help to candidates for A.O.C.P.

D.C./D.C. Power Supplies for Mobile, GSKRY. Two inverter circuits.

V.K.1, Criss, H.M.S. London, GJFFJ/MM. Readers of "A.R." will remember that Mike Matthews, Chief Radio Supervisor in H.M.S. London, visited Melbourne and other Australian cities during January 1970.

April 1970.

Monitor for T.V.I., GHEI. A device for continuously checking the transmitter during operation.

Some Useful Circuits for Your Notebook, GSHP. 0-10 volts, regulated p.a.u. at 1 amp.

ULVU Audio Peak Limiter for A.M./S.S.B., ZLALC. Two-Tone Test Oscillator GMRAPX Wide Band Signal Injector.

The New Marconi RM600 Sophisticated professional receiver covering the frequency range 15-30 MHz.

Testing Out on Two Bands, GSVLC. Even if you have a small back yard, you can still produce a signal on 180 metres.

How to Use the Transmitter, GGOGR. Uses up some surplus valves to run ten watts input on 160 and provide power for the serials described above.

Translating Bug Key, GJPFV. Simple PET Voltmeter, SVH.

"THE AUSTRALIAN E.E.B."

Over a number of years the name of R. L. Gumbert has been in relation to various Amateur matters in Tasmania and also in respect of a small, newsy and informative publication known as "The Australian E.E.B." (Electronic Experimenter's Bulletin). Occasionally I saw a copy of the publication and had the opportunity of examining its contents.

During the latter part of April I happened to be visiting V.I. on business and had the good fortune to meet Dr. Leo Gumbert at the Hobart Technical College. Arrangements have been made for copies of "The Australian E.E.B." to be sent regularly for review. I feel certain that the Amateur who is experimentally minded will find much to interest him in this publication.

February 1970—

Photophones for the Amateur, VKIDZ. Deals with short distance communication using modulated light.

Further Notes on High Quality Receiver Design, Heding, VK3. Describes the design and operating principles of the Pleassey PR155, solid state, general purpose, communications receiver frequency range 80 KHz. to 30 MHz.

Review, R.L.G. reviews the contents of '73 Diode and Long Wire Antennas."

Regulated T.V. Power Supply Design, VKTNG. Part 1, describes the following: components, Basic design details, curves, etc., are given.

March 1970—

A Nice Hi-Fi Amplifier System, Part 1, A. Whittingham (VK3). Uses a unit of commercial design available from Philips, Mullard or Fairchild and capable of an output of about 50 W.

Valveless Transmitter, VK3. The Australian L. S. Thomas (VK6) Must Amateurs are car owners.

Transformer Rejuvenation, H. Bracken, VK-TBR. Some of those old transformers you have had stored under your house may need some attention before they are put back into service.

SCR Two-Period Timer, E. Kershaw (VK3). A useful, old switching device.

Regulated Low Voltage Power Supply Design, Part 2, R.L.G. Takes you on from where we left off last month. More curves, diagrams and elaboration.

April 1970—

A Nice Hi-Fi Amplifier System, Part 2, Putting a box around the bits.

SCR Filter, L. J. Yelland (VK3). If your pulse is wavering, try this.

When Noise Interferes, E.A.O. Carver (VK3 Anon). Things are not always what they seem to be.

Amplifier (Xerix) Type Transistor Ignition, K. H. Vierz (VK4) To make your bomb a hot performer.

The Legal Position on Light Beam Communications, Staff. Conclusion: "even a torch should be licensed" (Monopoly gone mad!!!)

Wideren Wiper Delay System, L. E. Thom. The delay system is not limited. I wonder if this author was one of the occu-

points of a Morris B.M.1 once saw, soon after their release by H.M.C. with the sign in the rear window, "Transistorized Rolls Royce".

Continuously Variable Windscreen Wiper Speed, R.L.G. and G.R.J. More on a similar subject.

L.V. Regulated Power Supply Design, Part 3, R.L.G. Battery makers beware.

A Crystal Checker and Frequency Comparator for V.R.F., I. N. Kallam (VK3). Where will technology stop?

One of the things I like about "E.E.B." is its uninhibited approach to things. Much good advice on electronics and general topics of interest to the modern Radio Amateur.

Obtainable from "The Australian E.E.B." P.O. Box 177, Sandy Bay, Tasmania, 7008. Price 25c. per copy, 1 year \$1, 3 years \$3. (eight issues yearly).

"73"

March 1970—

Extra Services from Your Grid Dip Oscillator, WA4UZZ. Like checking crystals, tuning fm receivers and such.

A Reverse Current Charging, KAYUC. Turns out you really can re-charge flashlight batteries. (A good technique, if it works. Triers please report.)

A Few Men's Frequency Meter, WGYAN. Combines surplus from two services.

Professional PCs from Roll-Your-Own Negs, KEMVH. Eliminates drafting. Camera work and dark room entirely.

How I Read the RO's Handbook and Found Happiness, Johnston. Instant profundity.

A Look at Amateur F.M. Standards, WBSDT. Or, how do we get out of this mess.

An Inexpensive R.F. Wainmeter, WB4MYL. Surplus meter for those too cheap to buy a regular wainmeter.

A Remote Multi-Frequency Oscillator for Surplus F.M. Units, WIACMC. Drive people crazy on lot more fm channels with this.

Asse Spelling to Your F.T.O., KEMVO. If your V.L.O. is unspotted.

Towards an Ideal Solid State I.F. for Amateurs, R.L.G. Closing in on the state of the art with Bill Hossington.

Ham Exchange, WAZELA. Visiting foreign Amateurs makes trips more enjoyable.

Radio Star, WAZAQ. Heath wouldn't recognize it.

Bob, Bob, Bobbin' Along, K1YBD. Special April feature article.

The Big Little VESUCE. A grid-dip meter with no grid and no meter.

"73" Checks Out the Krtis Scanning Receiver, Staff.

A C.W. Monitor, WB2QY. Using a 680 audio module, you cheapskates.

The Logical Approach to Surplus Buying, Jim Kopy. Here's your key to fun with those surplus logic circuits.

Converting the Soneberry to a SW. F.M. Rig, W1WYC. Two metres, why not have some fun with this one.

Easy Diode Testing, K&K. Checking out those bargain diodes.

Tuning the AN/GEC-3 into a Navies Rig, WJETT. 3-12 MHz transmitter-receiver. If it does not work, check c.t. of rx ht. supply—V.I. says!

Extra Class Study Course, Part 14, Staff. Measurements.

V.I. and F.M. and You, K3DTH. Part of our Encyclopedia of F.M.: a good part.

April 1970—

The banner headline proclaims this a "Special F.M. Repeater Issue".

A Noise Blaster That Works, WERHR. As opposed to that crummy one on Brand X which doesn't work. Can't you add to your present receiver easily. (On p. 18 the author acknowledges that he pinched the circuit from R. L. Drake 1.)

Hot Carrier Diode Mixer Converter, WABNCT. This is not an April Fool article.

Examining F.M. Repeater Operation, WBEJFT. History repeats, A.R.E.L. Involvement and legal problems.

A Repeater Controller, WA4YND. Tone generator timer, identifier, the lot.

Understanding the Carrier Operator Repeater, KEMVH. Some of them take a good deal of understanding.

Evaluation, Standard 3 Metres F.M. It-Channel Receiver, WQGNK. Okay.

1/8 Wave Mobile Antenna for Two Metres, WZEPW. Why have a puny signal when you can have a megawatt signal.

How Do Ham Stores Decide Their Trade-In Figures, WZCWP. \$200 for your 538?

Scruffy, the Official Refractory, WBSAP. Worms that illuminate.

Getting Your Extra Class License, Part 15, Staff. Spurious radiation is covered.

A Word to Setters on the Wielda Repeater, WODKU. If anything can go wrong . . .

Inexpensive Semiconductors for the Ham, WATERE. Glan Motorola the fact that we paid for

Renovating Surplus Meters, WABAB. Making new scales, calibrating, etc.

A More Repetitive Than the ZL2ANG Simple gadget that makes class B practical.

High Performance I.F. and A.G.C. System, ZL2HDB. Particularly for c.w. and s.s.b.

Slideband on the All-Wave Radio, WICSD. One transistor b.l.o. and no connections.

Vacuum Tube Load Box, Jim Ashe. Invaluable for testing power supplies. (During 1963 a similar device using 6L6s was built for use by the Army Apprentices School, Bomber Victoria. It was only designed to pass a current of about 150 mA. Had 80% been used the current could have been run up to 200 mA. About 700 volts about 700 mA. A versatile device for testing power supplies with current outputs up to about 1 amp, can be constructed by using four series strings of 90-250 volt lamps which can be connected in parallel with suitable switches with a unit similar to that described for fine adjustment between steps.

WJASBC.

Repeater Directory, Staff. Special feature giving details of the U.S. repeater locations, frequency, etc.

A Word About Repeaters, WBAEB. A special feature.

The Five Points of F.M. Operation, WBAEB. Getting on frequency and other fine points.

How to Migger Your Antenna, WZEEY. It's not too dirty.

★

S.A.A. REPORTS

SAFETY OF TELECOMMUNICATIONS EQUIPMENT (TE/1)

A working group met in April to complete the details of a revision of AS C159-1960 Ap. of revised 760 volts and 1000 volts, with specific comment being sought on various sections of the draft that cannot yet be resolved. For example, the problem of applying the safety and high voltage tests to equipment containing solid-state circuitry is left to require a new approach.

RADIO INTERFERENCE (TE/3)

At the April meeting of this committee, the main subject under discussion was the setting of acceptable limits for local oscillator radiation from television receivers. The problems of measurement, of manufacturing within limits, and of affording the protection required by other services, were found to be very considerable but compromise proposals will be incorporated in a draft to be issued for public review and further investigation will proceed in the meantime. The concept of "immunity" as it applies to t.v. receivers was discussed at some length, and a working group was appointed to study a method of measurement.

RADIO COMMUNICATION (TE/14)

This committee at its last meeting broke up into three sub-committees dealing respectively with radio reception, radio transmission, and serials, and the sub-committee meetings produced a number of proposals. A joint meeting was held at which progress in the sub-committee sections was reported, and guidance was given regarding further work at the sub-committee level.

(Reprinted from the Standards Association of Australia May 1970 Monthly Information Sheet.)

★

PROVISIONAL SUNSPOT NUMBERS

MARCH 1970

Dependent on observations at Zurich Observatory and its stations in Locarno and Arosa.

Day	R	Day	R
1	134	18	48
2	134	19	48
3	113	20	48
4	161	21	48
5	167	22	53
6	190	23	115
7	168	24	122
8	116	25	131
9	123	26	140
10	123	27	141
11	100	28	122
12	104	29	115
13	104	30	111
14	84	31	103
15	88	32	111
16	102	33	101

March 1970 Mean equals 161.7
Smoothed Mean for Sept. 1969 165.8
Swiss Fed. Observatory, Zurich.

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Solari 24-Hour Digital Clocks.
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- Range 3—46-76 MHz.
- Range 4—27-46 MHz.

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Stability: 1 part in $10^6/^{\circ}$ C. (free running).
1 part in $10^6/^{\circ}$ C. (crystal controlled).

Intermediate frequency: 10.7 MHz.

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Crystal calibrator: 10 MHz. markers.

MODEL 990S

Frequency coverage:

- Range 1—470-870 MHz.
- Range 2—230-510 MHz.

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- AM: 5 μ V. for 10 dB. S/N (1 MHz. B/W).
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1 MHz. FM.

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Crystal calibrator: 50 MHz. markers.

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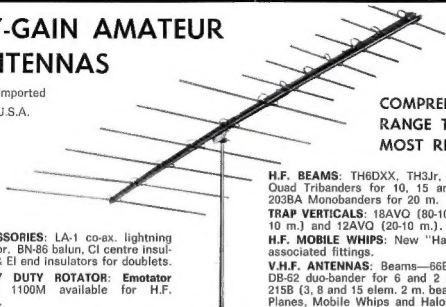
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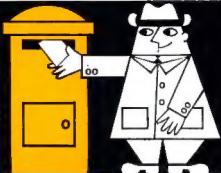


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